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# Vulnerability of Some Fairbanks North Star Borough Schools to Earthquake Damage Based on Rapid Visual Screening

June 15, 2017

Prepared for:

Administered by: Funded by:

Fairbanks North Star Borough School District and Alaska Seismic Hazards Safety Commission The Earthquake Engineering Research Institute Federal Emergency Management Agency



The Federal Emergency Management Agency (FEMA)



The Department of **Homeland Security** (DHS)



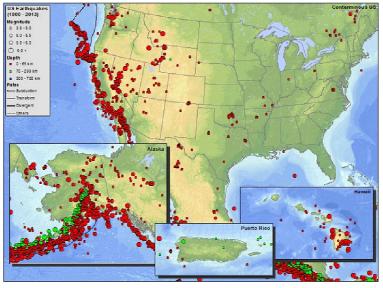
The Earthquake **Engineering Research** Institute (EERI)



The Alaska Seismic Hazards Safety Commission (ASHSC)

### **Alaskan Seismicity:**

Alaska is among the most seismically active areas on Earth. Over the past 50 years, the United States Geological Survey (USGS) recorded in the United States more than 3,000 earthquakes more powerful than magnitude 5, with approximately 80% of these occurring in Alaska. Further, of twelve powerful the most earthquakes America has ever experienced, ten were situated in Alaska. These include the 1964 Great Alaska Earthquake, which remains the second most powerful ever measured on Earth.



Sites of major earthquakes in the US (USGS)

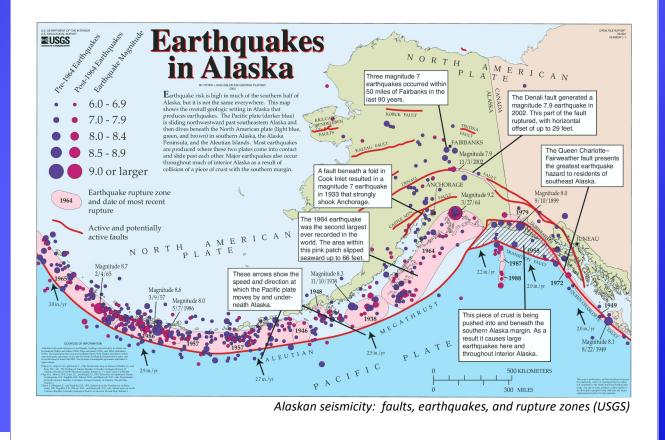
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Alaska's intense seismicity is a result of plate tectonics. The Pacific Plate, moving north 2" to 3" per year, slides below the North American Plate at a fault called the Aleutian Megathrust. This tectonic collision and subduction is able to produce an earthquake up to magnitude 9.2, according to the Federal Emergency Management Agency (FEMA). Many other faults occur around the state, and though earthquakes associated with them are not as powerful, they may govern the nearby ground accelerations because of their close proximity.

The strength and duration of Alaska's 1964 earthquake shocked the scientific world, spurring an increase in

3-D Model of the Aleutian Megathrust sliding below the North American Plate (USGS)

research in plate tectonics and seismology. The Alaska Dispatch News chronicled many of these changes in a March 23, 2014 article on the subject: "The 1964 event changed the way we thought about earthquakes,' said Mike West, state seismologist with the [Alaska Earthquake Center] at the University of Alaska Fairbanks. 'It literally helped prove plate tectonics.'"



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### **Building Codes:**

Similarly, the 1964 Alaskan earthquake substantially changed the way building structures are designed. In 1973, the Uniform Building Code was modified to add many new, specific

requirements. For example, descriptions of seismic force collectors within floors and roofs were added, as were new detailing requirements for seismic safety in regions of high seismicity. Design seismic forces for braced frames effectively doubled; unreinforced masonry and concrete were now prohibited for all structural elements in regions of high seismicity; gravity-only columns now needed to be designed to have sufficient strength when swaying dramatically during a seismic event.



Concrete column failure, West High School, Anchorage, AK After 1964 Great Alaska Earthquake

Since then, building codes have continued to be modernized. In response to observations after other earthquakes and informed by extensive testing, building code committees have continued to increase design seismic forces, establish more robust detailing requirements, and intensify inspection mandates. Schools in particular are now designed for an increased factor of safety because of their importance to their communities. Further, in some cases schools are designed to an even higher level of safety so they can be used as shelters following a major earthquake. Because of these changes and many others, buildings constructed today are much more earthquake-resistant than older buildings.

The fact that older buildings are less earthquake-resistant is significant to Alaskan schools because many of them were constructed before building code modernization began to improve the safety of building construction. As a result, older school buildings are typically less earthquake-safe than newer ones. How much less safe depends on many factors, including age and type of structural system, structural irregularities, building location, and quality of construction. School districts and managers of facilities would benefit greatly from having good information readily available regarding the safety of their facilities. This would enable them to make informed decisions regarding timing and urgency of any further structural reviews and upgrades.

### **Rapid Evaluation of Facilities:**

To that end, FEMA developed a rapid evaluation procedure outlined in their publication P-154, "Rapid Visual Screening of Buildings for Potential Seismic Hazards: A Handbook." This contains a method for evaluating structures' seismic performance very quickly and without great expense, referring to it as a "sidewalk survey." It takes into account the age and type of structure, building height, irregularities in the structure that decrease reliability, and whether it was constructed before the enforcement of design codes and the implementation of construction inspection. FEMA

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developed this method to provide a tool to give building owners and managers good, actionable information with minimal up-front cost.

The method used by FEMA P-154 to evaluate a building is quite straightforward. It establishes an initial score for each type of structural system (wood shear walls, steel braced frame, and so forth), with a higher score indicating greater reliability. A given building's initial score is then modified (up or down) based on other factors, including the number of stories, vertical structural irregularities, plan structural irregularities, probable soil type, whether it was designed and constructed before codes were generally enforced, and whether it was designed and constructed under substantially modern codes. The user enters the building information, adding and subtracting from the initial score to obtain the final score. FEMA carefully selected the scores and modifications so the final score could carry some readily understandable information. The Third Edition of FEMA 154 notes, in section 5.2:

Fundamentally, the final S score is an estimate of the probability (as described in Chapter 1) if an earthquake occurs with ground motions called the risk-targeted maximum considered earthquake,  $MCE_R$ , as described in Chapter 2...

A final score, S, of 3 implies there is a chance of 1 in  $10^3$ , or 1 in 1,000, that the building will collapse if such ground motions occur. A final score, S, of 2 implies there is a chance of 1 in  $10^2$ , or 1 in 100, that the building will collapse if such ground motions occur.

BBFM Engineers makes no statement about these probabilities except to note FEMA's intent in developing the scoring process. Typically a final score below 2.0 is taken as indication that a more detailed investigation is warranted, although that value can be adjusted at the outset of an evaluation project as desired by the owner of the facilities.

Importantly, these scores and risks do not take into account actual member strengths or actual connection reliability, only what is common for similar structural types of similar age. Therefore, the actual building safety may be substantially different from what the scores may indicate. Accordingly, buildings with low scores are noted as requiring further structural investigation to determine whether structural upgrade is warranted. These scores can be used appropriately to identify and rank buildings for their vulnerability to earthquake damage.

### Alaskan School Safety:

As stated in 2010 by the Western States Seismic Policy Council (WSSPC), "Every community is required to educate children, and it is the responsibility of governmental agencies to design and construct safe buildings to house them. While current building codes and construction practices have recognized the effects of earthquakes and provide state-of-the-art design considerations, many older school buildings were built before these principles were understood... These older buildings have not been properly graded or passed the test of seismic safety. Consequently, many students face significant seismic risk." The WSSPC is a non-profit consortium of eighteen member states and territories including Alaska.

After all, since children are required to attend school and parents lack specific information about the seismic safety of different structures, it is the responsibility of the government to ensure the

schools provide a safe learning environment for Alaskan children. Again, schools may be used as emergency shelters after major earthquakes, further raising the importance of the building's successful performance during an earthquake.

According to the Alaska Department of Education, the total enrollment in public school districts in Alaska as of October 1, 2016, was 133,223. Of these, 13,840 students are in the Fairbanks North Star Borough School District, or about 10.5% of the state's total. School districts statewide accept as part of their mission to protect the safety of children as well as facilities whose replacement cost is many billions of dollars.

### This Study:

In the interest of student safety and community resilience to earthquakes, BBFM Engineers was asked to perform a rapid visual screening of several aging schools in the Fairbanks North Star Borough School District to determine which schools warrant an in-depth seismic review, and which structures are expected to perform acceptably during a major earthquake. The screening program follows the criteria established by FEMA Publication 154, Third Edition. FEMA refers to this screening program as a "sidewalk survey" because it is intended to be a very quick review of structure type, structure age, structural discontinuities, local seismicity, and the like.

In this study, BBFM Engineers completed the screening of ten schools, most of which have several additions. In total, we reviewed twenty structures, including original construction and additions. In surprising contrast to other school districts reviewed previously, all twenty warrant a more detailed evaluation. A primary reason for this is that most of the schools resist seismic forces using concrete, precast concrete, or masonry shear walls, and older systems of these types have not performed well in past major earthquakes.

In addition to further review of the twenty schools, we also recommend that similar studies be undertaken in all regions of high seismicity throughout the state, especially in light of the cost-effectiveness of the FEMA 154 process, which can be performed for just \$700 to \$1,200 per structure. Studies including many structures in readily accessible areas may find economies allowing them to be performed for fees near the lower end of this range, while remote or smaller-scale studies may require a higher fee.

## **Objectives of this Study:**

This study was funded by FEMA and managed by the Earthquake Engineering Research Institute (EERI) and the Alaska Seismic Hazards Safety Commission (ASHSC). It is the goal of FEMA and of EERI to improve earthquake safety throughout the country, and to that end they are sponsoring projects in various states to showcase the ease and value of rapid visual observation of schools.

Two goals reside at the core of this study: to show planners how quickly and cost effectively an initial assessment can be performed for schools using FEMA's rapid visual screening program, and to rate a sampling of existing schools to provide the Fairbanks North Star Borough School District information crucial to their planning purposes. Any buildings of concern can then be prioritized for further study and/or upgrade, as appropriate.

ASHSC looked for a school district with older schools constructed with a variety of structural

system types and found a willing participant in the Fairbanks North Star Borough School District, home of some 10.4% of Alaska's pre-kindergarden through 12th grade students. BBFM reviewed the following ten schools:

- 1) Barnette Elementary School (1960 original and 1970 and 1974 additions)
  - Hunter Elementary School (1956 original and 1957, 1958, 1959, and 1974 additions)
- 3) Hutchison Career Center

2)

- (1973 original and 1975 addition)
- 4) Joy Elementary School (1971 original)
- 5) Lathrop High School (1953 original and 1957, 1962, and 1970 additions)
- 6) North Pole Elementary School (1967 original)
- 7) North Pole Middle School (1975 original
- 8) Tanana Middle School (1974 original)
- 9) West Valley High School (1976 original)
- 10) Woodriver Elementary School (1976 original)

BBFM Engineers visited the school district's plans room and copied all available structural drawings. Before we visited the schools themselves, we began a FEMA P-154 data collection form for each structure, inputting all available information: location in relation to known seismic faults, structural system type, year of construction, and more.

BBFM Engineers then visited the schools, photographing their current condition and noting any conditions not shown on the drawings and materials that, during an earthquake, could become pounding or falling hazards. In this manner, all the information necessary for the Rapid Visual Screening was obtained.

The final report can be found along with previous RVS reports on the ASHSC website at: http:// seismic.alaska.gov/presentations\_reports.php. Upon approval by the Fairbanks North Star Borough School District, the plans, photos, and other supporting information can also be provided in electronic format, which may prove valuable for further building assessment or post-earthquake response. Requests for supporting information should be made to the Alaska Seismic Hazards Safety Commission or BBFM Engineers.

### Cost of this Study:

The grant awarded by FEMA and managed by EERI was \$25,000. After administrative overhead, BBFM's fee was \$21,250 for the review of twenty structures (original construction plus additions). Extrapolating for future studies, similar Rapid Visual Screening could be performed at a very minimal cost, approximately \$700 to \$1,300 per original structure or addition, depending on availability of drawings, ease of access to the schools, and number of schools being included in the study. This cost can even be applied to schools off the road system if the school staff provides electronic photographs, although a generous schedule may be necessary to ensure photographs arrive in time for related information to be included in the report.

We uploaded the available structural drawings for all the schools, along with photographs and FEMA P-154 Data Forms onto the cloud, as these could be very useful after a major earthquake. The drawings are in multi-page .pdf format, the standard format for the industry, while the drawings are in .jpg format.

### Results of the Study:

Of the twenty structures reviewed, the final scores range from 0.9 to 1.9. According to FEMA's guidelines, these represent estimated probabilities of partial or complete collapse of 13% and 1.3%, respectively. These probabilities are dramatically impacted by building design and construction practices common at the time, which may differ significantly from the practices used on these particular structures.

Again, all twenty structures exhibited scores below 2.0, indicating a more detailed investigation of the structure is necessary. Further, some of the schools also have potential hazards from falling chimneys or pounding hazards from adjacent canopies that should be investigated in greater detail.

Following are the results for each school, sorted in alphabetical order. Following these results, we have also sorted the schools by final score, which may assist in prioritization of further work.

- 1) Barnette Elementary School: 1960 Original Construction
  - Reinforced concrete shear wall construction
  - Final score = 1.2; FEMA estimate of collapse risk: 6%
  - Detailed investigation is indicated for structural design and detailing.
  - Detailed investigation is indicated for the unbraced chimney.
  - Detailed investigation is indicated for the canopy at exterior doors of rooms 301 and 302.
- 2) Barnette Elementary School: 1970 Addition
  - Reinforced concrete shear wall construction
  - Final score = 1.2; FEMA estimate of collapse risk: 6%
  - Detailed investigation is indicated for structural design and detailing
- 3) Barnette Elementary School: 1974 Addition
  - Wood frame and reinforced concrete shear wall construction
  - Final score = 1.2; FEMA estimate of collapse risk: 6%
  - Detailed investigation is indicated for structural design and detailing
- 4) Hunter Elementary School: 1956 Original Construction
  - Reinforced concrete shear wall construction
  - Final score = 1.2; estimate of collapse risk: 6%
  - Detailed investigation is indicated for structural design and detailing
- 5) Hunter Elementary School: 1957 Addition
  - Wood frame and reinforced concrete shear wall construction
  - Final score = 1.2; estimate of collapse risk: 6%
  - Detailed investigation is indicated for structural design and detailing
- 6) Hunter Elementary School: 1958 Addition
  - Reinforced concrete shear wall construction
  - Final score = 1.2; estimate of collapse risk: 6%
  - Detailed investigation is indicated for structural design and detailing
- 7) Hunter Elementary School: 1959 Addition
  - Reinforced concrete shear wall construction
  - Final score = 1.2; estimate of collapse risk: 6%
  - Detailed investigation is indicated for structural design and detailing

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- 8) Hunter Elementary School: 1974 Addition
  - Wood frame construction
  - Final score = 1.9; estimate of collapse risk: 1.3%
  - Detailed investigation is indicated for structural design and detailing
- 9) Hutchison Career Center: 1973 Original Construction
  - Reinforced masonry construction
  - Final score = 1.0; FEMA estimate of collapse risk: 10%
  - Detailed investigation is indicated for structural design and detailing.
- 10) Hutchison Career Center: 1975 Addition
  - Reinforced masonry construction
  - Final score = 1.0; FEMA estimate of collapse risk: 10%
  - Detailed investigation is indicated for structural design and detailing.
- 11) Joy Elementary School: 1961 Original Construction
  - Reinforced concrete shear wall construction
    - Final score = 1.2; FEMA estimate of collapse risk: 6%
    - Detailed investigation is indicated for structural design and detailing.
  - Detailed investigation is indicated for the unbraced chimney.
- 12) Lathrop High School: 1953 Original Construction
  - Reinforced masonry and reinforced concrete shear wall construction
  - Final score = 1.0; FEMA estimate of collapse risk: 10%
  - Detailed investigation is indicated for structural design and detailing.
  - Detailed investigation is indicated for the unbraced chimney.
- 13) Lathrop High School: 1957 Addition
  - Reinforced masonry and reinforced concrete shear wall construction
  - Final score = 1.0; FEMA estimate of collapse risk: 10%
  - Detailed investigation is indicated for structural design and detailing.
- 14) Lathrop High School: 1962 Addition
  - Reinforced masonry and reinforced concrete shear wall construction
  - Final score = 1.0; FEMA estimate of collapse risk: 10%
  - Detailed investigation is indicated for structural design and detailing.
- 15) Lathrop High School: 1970 Addition
  - Reinforced masonry and reinforced concrete shear wall construction
  - Final score = 1.0; FEMA estimate of collapse risk: 10%
  - Detailed investigation is indicated for structural design and detailing.
- 16) North Pole Elementary School: 1967 Original Construction
  - Wood frame and reinforced masonry shear wall construction
  - Final score = 1.0; FEMA estimate of collapse risk: 10%
  - Detailed investigation is indicated for structural design and detailing.
- 17) North Pole Middle School: 1975 Original Construction
  - Reinforced masonry shear wall construction
  - Final score = 1.0; FEMA estimate of collapse risk: 10%
  - Detailed investigation is indicated for structural design and detailing.
- 18) Tanana Middle School: 1974 Original Construction
  - Reinforced masonry shear wall construction
  - Final score = 1.0; FEMA estimate of collapse risk: 10%
  - Detailed investigation is indicated for structural design and detailing.

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- 19) West Valley High School: 1976 Original Construction
  - Steel braced frame, precast concrete, and reinforced masonry shear wall construction
  - Final score = 0.9; FEMA estimate of collapse risk: 13%
  - Detailed investigation is indicated for structural design and detailing.
- 20) Woodriver Elementary School: 1976 Original Construction
  - Steel braced frame, precast concrete, and reinforced masonry shear wall construction
  - Final score = 0.9; FEMA estimate of collapse risk: 13%
  - Detailed investigation is indicated for structural design and detailing.

For the sake of prioritization, it may be convenient for the school district to see the ten different facilities sorted by the FEMA estimate of the risk of collapse or partial collapse. That information is provided below.

West Valley High School Woodriver Elementary School	13% FEMA Risk 13% FEMA Risk	
Hutchison Career Center Lathrop High School North Pole Elementary School North Pole Middle School Tanana Middle School	10% FEMA Risk 10% FEMA Risk 10% FEMA Risk 10% FEMA Risk 10% FEMA Risk	(Also, unbraced chimney)
Barnette Elementary School Hunter Elementary School Joy Elementary School	6.3% FEMA Risk 6.3% FEMA Risk 6.3% FEMA Risk	(Also, canopy, unbraced chimney) (Also, unbraced chimney)

With relatively little time or expense, this study has identified many structures that may perform poorly during a major earthquake. The schools appear to pose a significant risk to students in the Fairbanks North Star Borough School District and to the communities they serve. All twenty of the original buildings and additions were flagged as requiring further structural attention. In other words, they may pose an unacceptable risk of at least partial collapse during a major earthquake. Following FEMA Publication 154, the four largest contributors to a building's seismic risk are: a) common industry practices when the structure was built, b) type of structural system, c) the presence of and type of structural irregularities, and d) the seismicity of the region.

The study of these schools in the Fairbanks North Star Borough School District indicates there would be great value in conducting similar studies statewide, where more than 500 public schools serve kindergarten through twelfth grade. It is the responsibility of school districts and school boards, as well as local and statewide governing bodies to reduce the risk earthquakes currently pose to students and facilities alike, and this rapid evaluation method would quickly and economically identify those structures requiring further attention.

In a December 17, 2014, interview aired by the Alaska Public Radio Network, Alaska Governor Bill Walker pointed out that the tightness of today's Alaskan economy requires policymakers to be particularly focused on our state's priorities, and that education is a high priority. Fortunately, structural review and upgrade is truly one area where "a stitch in time saves nine." Over time, the

cost of not upgrading a deficient structure typically exceeds the cost of improving the structure before a major earthquake hits, and even more so when lives and disruption to society are factored in.

### **Effectiveness of Seismic Retrofit:**

Various earthquakes have shown that seismic retrofits to a building can substantially improve its performance during a major earthquake. For example, the 2001 Nisqually Earthquake near Olympia, Washington produced peak ground accelerations 10% to 30% as strong as the acceleration due to gravity. Reviewing the aftermath, the California Seismic Safety Commission determined that "One hundred and one schools and buildings had been retrofitted for structural components and seven had been retrofitted for non-structural components in the Seattle Public Schools District when the Nisqually earthquake occurred. None of the districts schools suffered significant structural damage. Non-structural damage to colleges and universities included toppling of bookcases and the localized flooding due to a ruptured water line. Some primary and secondary schools in Olympia and Seattle suffered limited structural (damaged beams and columns) and non-structural damage from strong ground shaking."

A second example is the magnitude 6 earthquake that struck Napa, California in 2014, producing peak ground accelerations of 60% to 100% as strong as the acceleration due to gravity. The earthquake and its aftershocks injured 90 people and caused approximately \$1 billion of damage. Engineering News-Record reported on September 3, 2014:

The epicenter of the American Canyon quake was at the heart of the Napa school district's 30 campuses. Subsequently, three architectural and engineering teams assessed "every room in every school" and observed no structural damage following the quake, says Mark Quattrocchi, principal of Kwok Quattrocchi Architects and one of the survey team members... The schools performed so well because they are built or retrofitted according to much stricter seismic codes than commercial and residential buildings.

"There was no structural damage to any school in the district, even the ones built to older codes in the 1940s, 1950s and 1960s," says Quattrocchi. "Part of this is because seismic upgrades at the schools are treated the same as building an entirely new facility," he adds.

Schools fared well for three reasons: seismic building codes that are more stringent than those for commercial buildings, methodical reviews by the Division of the State Architect and "full-time" state inspection on school construction sites, Quattrocchi says."

For buildings shown to be vulnerable to collapse during earthquakes, seismic retrofit can substantially improve the buildings' performance during a major earthquake.

Further, grants may be available from FEMA and other groups to facilitate seismic upgrades to school buildings.

### **Recommendations:**

We urge planners and policymakers to implement a program to assess rapidly and inexpensively the vulnerability of schools to earthquakes, both for the safety of the students and to protect financial investments across the state. The cost would be approximately about \$700 to \$1,200 per original structure or addition, depending on availability of drawings, ease of access to the schools, and number of schools being included in the study.

We also encourage further structural review for the twenty structures identified in this report as posing unacceptable seismic risk. That review should performed by a qualified structural engineering firm and should include a careful review of the specific loads, members, and connection details specific to these structures. Where appropriate, this additional analysis should include preliminary recommendations for structural upgrade, which can be fleshed out under a separate contract for preparation of construction documents.

For the safety of the students and to protect financial investments across the state, we urge planners and policymakers to implement a program to assess rapidly the vulnerability of schools to earthquakes. This program can be surprisingly inexpensive, costing as little as \$700 to \$1200 per structure, while effectively indicating which structures would or would not require further review. An added benefit of this process is that we have developed a database of photographs, structural plans, and other critical information and placed it on the cloud, where it will be readily available after a major earthquake. We also encourage further structural review and possible seismic retrofit for the twenty structures identified in this report as requiring a more detailed investigation.

**BBFM Engineers** 

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Rapid Visual Screening of Fairbanks North Star Borough Schools for Seismic Risk

Appendix A

FEMA P-154 Third Edition Data Collection Forms

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## Barnette Elementary School: 1960 Original Construction

### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

	Fairbanks, Alaska       zip:       99701         Other Identifiers:       Building Name:       Barnette Elementary School 1960 Original         Use:       school       147.7303 deg         Ss:       0.992       sr:       0.378         Screener(s):       SMG       Date/Time:       February 20         No. Stories:       Above Grade:       2       Below Grade:       0         Year Built:       1960       Code Year:       1958         Additions:       None       Xi Yes, Year(s) Built:       1970,       1974         Occupancy:       Assembly       Commercial       Emer. Services       Historic       Shelt         Industrial       Office       Utility       Warehouse       Soit       Soit       Por         Soil       Type:       A       B       Derse       Soit       Soit       Mok, assume Type         Rock       Rock       Soit       Soit       Soit       Soit       Soit       Mok, assume Type         Geologic Hazards:       Liquefaction:       Yes/No/DNK       Landslide:       Yes/No/DNK       Sundslide:       Yes/No/DNK Surf. Rupt.: Yes/No/DNK         Adjacency:       Xi Pounding       Falling Hazards from Taller Adjacent Building   <
	Building Name:       Barnette Elementary School 1960 Original School         Use:       School         Latitude:       64.8382 deg N         Latitude:       64.8382 deg N         Ss:       0.992         Sr:       0.378         Screener(s):       SMG         Date/Time:       February 20         No. Stories:       Above Grade: 2         Below Grade:       0         Year Built:       1960 r         Code Year:       1958         Additions:       None         None       Yes, Year(s) Built:         1970, 1974       Occupancy:         Occupancy:       Assembly         Commercial       Emer. Services         Industrial       Office         School       Government         Warehouse       Residential, # Units:         Soil Type:       A         Hard       Avg         Rock       Rock         Soil       Soil         Soil       Soil         Geologic Hazards:       Liquefaction: Yes/No         Botk       Industrial         Geologic Hazards:       Liquefaction: Yes/No
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	Jatitude:       64.8382 deg N       Longitude:       147.7303 deg         Latitude:       0.992       Sr:       0.378         Screener(s):       SMG       Date/Time:       February 20         No. Stories:       Above Grade:       2       Below Grade:       0       Year Built: 1960 r         Total Floor Area (sq. ft.):       38,000       Code Year: 1958       Additions:       None       No Stories:       Above Grade:       Year Year(s) Built:       1970, 1974         Occupancy:       Assembly       Commercial Industrial Office       Emer. Services       Historic       Shelt         Industrial       Office       Utility       Warehouse       Soft       Poor       Residential, # Units:         Soil Type:       A       B       C       D       Soft       Poor       NoK, assume Type         Rock       Rock       Soil       Soil       Soil       Soil       Soil       Poor         Geologic Hazards:       Liquefaction:       Yes/No/DNK       Landslide: Yes/No/DNK       Surf. Rupt.: Yes/No/DNK
	Ss:       0.992       Sr:       0.378         Screener(s):       SMG       Date/Time:       February 20         No. Stories:       Above Grade:       2       Below Grade:       0         Year Built:       1960 r       Code Year:       1958         Additions:       None       Yes, Year(s) Built:       1970,       1974         Occupancy:       Assembly       Commercial       Emer. Services       Historic       Shelt         Industrial       Office       Utility       Warehouse       Residential, # Units:       Soil       Soil       Foor         Soil Type:       A       B       C       D       E       F       F         Hard       Avg       Dense       Soil       Soil       Soil       Soil       Boll         Geologic Hazards:       Liquefaction: Yes/No/DNK       Landslide: Yes/No/DNK       Surf. Rupt.: Yes/No/DNK
	Screener(s):       SMG       Date/Time:       February 20         No. Stories:       Above Grade:       2       Below Grade:       0       Year Built:       1960 r         Total Floor Area (sq. ft.):       38,000       Code Year:       1958         Additions:       None       Yes, Year(s) Built:       1970,       1974         Occupancy:       Assembly       Commercial       Emer. Services       Historic       Shelt         Industrial       Office       Utility       Warehouse       Residential, # Units:       Soil       Soil       Poor         Soil Type:       A       B       C       D       E       F       DNK       I/DNK, assume Type         Rock       Rock       Soil       Soil       Soil       Soil       Soil       Gould Soil       Soil, Soil       Soil         Geologic Hazards:       Liquefaction:       Yes/No/DNK       Landslide: Yes/No/DNK       Surf. Rupt.: Yes/No/DNK       Surf. Rupt.: Yes/No/DNK
	No. Stories:       Above Grade:       2       Below Grade:       0       Year Built:       1960 r         Total Floor Area (sq. ft.):       38,000       Code Year:       1958         Additions:       None       None       Yes, Year(s) Built:       1970,       1974         Occupancy:       Assembly       Commercial       Emer. Services       Historic       Shelt         Industrial       Office       Utility       Warehouse       Residential, # Units:       Soil       Soil       For         Soil Type:       A       B       C       D       E       F       HMK, assume Type         Rock       Rock       Soil       Soil       Soil       Soil       Soil       Month, Surf. Rupt.: Yes/No         Geologic Hazards:       Liquefaction:       Yes/No.DNK       Landslide: Yes/NoDNK       Surf. Rupt.: Yes/No
	Total Floor Area (sq. ft.): 38,000       Code Year: 1958         Additions:       None       X       Yes, Year(s) Built:       1970, 1974         Occupancy:       Assembly       Commercial       Emer. Services       Historic       Shelt         Industrial       Office       School       Government       Residential, # Units:       Shelt         Soil Type:       A       B       C       D       E       F       DNK         Hard       Avg       Dense       Soil       Soil       Soil       Soil       Soil       F       DNK         Geologic Hazards:       Liquefaction:       Yes/No/DNK       Landslide:       Yes/No/DNK       Surf. Rupt.:       Yes/No/DNK
	Additions:       None       X       Yes, Year(s) Built:       1970, 1974         Occupancy:       Assembly       Commercial       Emer. Services       Historic       Shelt         Industrial       Office       Utility       Warehouse       Residential, # Units:       Soil Type:       A       B       C       D       E       F       DNK         Hard       Avg       Dense       Soil       Soil       Soil       Soil       B       C       D       Industrial       Industrial       DNK, assume Type         Geologic Hazards:       Liquefaction:       Yes/No/DNK       Landslide:       Yes/No/DNK       Surf. Rupt.:       Yes/No/DNK
	Occupancy:       Assembly Industrial Utility       Commercial Office Warehouse       Emer. Services       Historic       Shelt         Soil Type:       A       B       C       B       B       C       B       D       E       F       DNK If DNK, assume Type         Nork       Rock       Rock       Soil       Soil       Soil       Soil       B       C       C       D       E       F       DNK If DNK, assume Type       B       C       Soil       Soil       Soil       Soil       B       C       C       D       E       F       DNK If DNK, assume Type       Soil       Soil <td< td=""></td<>
	Industrial Utility     Office Warehouse     School     Government       Soil Type:     A     B     C     D     E     F     DNK If DNK, assume Type       Hard     Avg     Dense Rock     Soil     Soil     Soil     Soil     Soil       Geologic Hazards:     Liquefaction: Yes/No/DNK     Landslide: Yes/No/DNK     Surf. Rupt.: Yes/No/DNK
	Utility     Warehouse     Residential, # Units:       Soil Type:     A     B     C       Hard     Avg     Dense       Rock     Rock       Soil     Soil       Geologic Hazards:     Liquefaction: Yes/No/DNK
	Hard Avg Dense Stiff Soft Poor <i>If DNK, assume Type</i> Rock Rock Soil Soil Soil Soil Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt.: Yes/N
	Rock Rock Soil Soil Soil Soil Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt.: Yes/
	Geologic Hazards: Liquefaction: Yes/NoDNK Landslide: Yes/NoDNK Surf. Rupt.: Yes/
	Irregularities: Vertical (type/severity)  Plan (type) Reentrant corners
	Exterior Falling IV Unbraced Chimneys Heavy Cladding or Heavy Ver
	Hazards: Parapets Appendages
	Other:
	COMMENTS:
	Original construction contains reentrant corners.
	Canopy at exterior doors for rooms 301 and 302
	may be subject to pounding against the main
	building during a severe earthquake.
SKETCH	Additional sketches or comments on separate page
	IFIERS, AND FINAL LEVEL 1 SCORE, SL1           \$2         \$3         \$4         \$5         C1         C2         C3         PC1         PC2         RM1         RM2         URM
Know (MRF) (B	(BR) (LM) (RC (URM (MRF) (SW) (URM (TU) (FD) (RD) SW) INF) INF)
	2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.7 1.0
	-1.0 -1.1 -1.0 -0.8 -0.9 -1.0 -0.7 -1.0 -0.9 -0.9 -0.9 -0.9 -0.7 -0.6 -0.7 -0.6 -0.5 -0.5 -0.6 -0.4 -0.6 -0.5 -0.5 -0.5 -0.4
	-0.7 -0.9 -0.7 -0.6 -0.6 -0.8 -0.4 -0.6 -0.5 -0.5 -0.3 -0.4 -0.7 -0.7 -0.6 -0.7 -0.7 -0.4
	-0.6 -0.8 -0.6 -0.2 -0.4 -0.7 -0.1 -0.5 -0.3 -0.5 -0.5 0.0
	1.4         1.1         1.9         NA         1.9         2.1         NA         2.0         2.4         2.1         2.1         NA           0.6         0.1         0.6         0.5         0.4         0.5         0.3         0.6         0.4         0.5         0.3
	-0.4 0.2 -0.1 -0.4 0.0 0.0 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2
oil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 -0	-0.6 NA -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2
naam aank Bergamme na saa	0.5 0.6 0.5 0.5 0.3 0.3 0.3 0.2 0.2 0.3 0.3 0.2 1.2
NAL LEVEL 1 SCORE, SL1 ≥ SMIN:	1.2
XTENT OF REVIEW OTHER H	HAZARDS ACTION REQUIRED
Are There Ha	Azards That Trigger A Detailed Structural Evaluation Required?
	ructural Evaluation? Yes, unknown FEMA building type or other building potential (unless S <sub>L2</sub> > X Yes, score less than cut-off
oil Type Source: No geotech report cut-off, if	if known) Xes, other hazards present
eologic Hazards Source: No geotech report   Falling ha	hazards from taller adjacent 🔲 No
	c hazards or Soil Type F
EVEL 2 SCREENING PERFORMED?	ant damage/deterioration to
	detailed evaluation is not necessary
onstructural hazards? Xes X No	No, no nonstructural hazards identified X DNK
	ate the following: EST = Estimated or unreliable data OP DNK = Do Not Know
Where information cannot be verified, screener shall no	
Where information cannot be verified, screener shall no           agend:         MRF = Moment-resisting frame         RC = Reinforced concrete           BR = Braced frame         SW = Shear wall	
egend: MRF = Moment-resisting frame RC = Reinforced concrete	

## Barnette Elementary School: 1970 Addition

### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

Partbanks, Alaska       zp:       99701         Oher infeating Name:       Barnetite Elementary School 19/0 Addition         Building Name:       School         Building Name:       School         School       School <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>Add</th> <th>ress:</th> <th>1</th> <th>000 E</th> <th>Barne</th> <th>tte St</th> <th>reet</th> <th></th> <th>212</th> <th>1000</th> <th></th> <th></th>								Add	ress:	1	000 E	Barne	tte St	reet		212	1000		
Bailding Name:       BarnetTel:       EarnetTel:       Implicit       147.7303 deg 0.378         Bailding Name:       School       147.7303 deg 0.378       357       0.378         School       147.7303 deg 0.378       57       0.378       0.378         School       16,000       Contract       Year Weing Date										F	airba	nks, A	Alaska	а	Z	(ip: 99	9701		
ue:       School       Lenghuda:       147.7303 deg         Severentfy:       SMG       DataTime:       February 201         Severentfy:       SMG       DataTime:       February 201         Severentfy:       SMG       DataTime:       Derugary 201         Severentfy:       SMG       DataTime:       Derugary 201         Vertex       Severentfy:       SMG       DataTime:       Derugary 201         Vertex       Severentfy:       SMG       Derugary 201       Derugary 201         Vertex       Severentfy:       Severentfy:       Severentfy:       Derugary 201       Derugary 201         Severentfy:       Werkows       Derugary 201       Derugary 201       Derugary 201       Derugary 201         Severentfy:       Derugary 201       Derugary 201       Derugary 201       Derugary 201       Derugary 201         Severentfy:       Derugary 201       Derugary 201 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>Oth</td> <td>er Identi</td> <td></td>								Oth	er Identi										
Listude:       64.8382.deg N       Longitude:       147.7303.deg         Screent;       Since       0.92       S:       DateTime:       February 201         No. Stories:       Above Grade:       Betwork Grade:       DateTime:       February 201         No. Stories:       Above Grade:       Betwork Grade:       Company:       Aware Stories:       Betwork Grade:       Company:				_				Bui	lding Na				emen	tary S	schoo	197	0 Ad	dition	
Si:       0.992       Si:       0.378         Si:       0.992       Si:       0.400         Si:       Si:       Si:       Si:       0.992         Si:			TT	Lm	-	10.4		1.0	888 <del>1</del>				N			4	17 70	02 4-	20
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Total Figor Area (sq. ht;         Good Year: 1967           Colspan="2">Code Year: 1967           Code Year: 1967		6 - 6 <sup>4</sup>	ALC:	-						-		. 2	Pala	- X3	Section 2	Shi			
Addition:          () None (S) Yes, Yes, Yes, Yes, Yes, Yes, Yes, Yes,						- 4	*	100000						w Grade	. 0				
Industrial Office       Converses         Industrial Office       Converses         Set Type:       A       B       Converses         Set Type:       A       B       Converses         Set Type:       A       Addicency:       Point file       Converses         Set Type:       A       Addicency:       Point file       Converses         Set Type:       A       Colspan="2">Converses       Paints Hazards form Tark Agaent Building         Induction forms       rependances       Paints Hazards form Tark Agaent Building         Paints Hazards form Tark Agaent Building       Paints Hazards form Tark Agaent Building         Paints Hazards form Tark Agaent Building       Paints Hazards form Tark Agaent Building         Paints Hazards form Tark Agaent Building         Paints Hazards form Tark Agaent Building         Paints Hazards form Tark Agaent Building         Paints Hazards form Tark Agaent Building         Paints Hazards form Tark Agaent Building       Paints														uilt:	1970,			1001	
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Soil Type:       A       B       C													•		tial #11r		overnmer	nt	
Hidd       Kig       Disc       Soft       Pior       IDDK summer Type D.         Rock       Soft       Soft       Pior       IDDK summer Type D.       Soft       Soft       Pior       IDDK Summer Type D.         Rock       Soft       Pior       IDDK Summer Type D.       Soft       Pior       IDDK Summer Type D.         Rock       Soft       Pior								Soil	Type								NK		
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Adjacency:       Pounding       Falling Hazards from Taller Adjacent Bulding         Irregularities:       Vertical (type/sevent)       Event (type)       Peartingt         Irregularities:       Vertical (type)       Peartingt       Heavy Cladding or Heavy Venee         Parapels:       Parapels:       Heavy Cladding or Heavy Venee         Irregularities:       Other:       Parapels:       Heavy Cladding or Heavy Venee         Irregularities:       Other:       Other:       Parapels:       Appendages         Irregularities:       Other:       Comments:       Additional sketches or comments on separate page         BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1       Additional sketches or comments on separate page         BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1       Event With With With With With With With Wit			_		-	_		-									0.40	-1. V	A1.
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Know         (MRF)         (BR)         (LM)         (MRF)         (M			В	ASIC	SCOR	E, MC	DIFIE	RS, A	ND FIN	AL LE	EVEL	1 SCO	RE, S	L1					
asic Score       3.6       3.2       2.9       2.1       2.0       2.6       2.0       1.7       1.5       2.0       1.2       1.6       1.4       1.7       1.7       1.0         evere Vertical Irregularity, V1,       -1.2       -1.2       -1.2       -1.0       -1.0       -1.1       -1.0       -0.8       -0.7       -0.6       -0.6       -0.6       -0.5       -0.5       -0.6       -0.4       -0.6       -0.6       -0.7       -0.7       -0.7       -0.7       -0.7       -0.6       -0.6       -0.5       -0.5       -0.6       -0.7       -0.7       -0.1       -0.5       -0.5       0.5       0.6       0.0       -0.7       -0.3       N.0       -0	EMA BUILDING TYPE		W1	W1A	W2				(RC	(URM			(URM		PC2			URM	
foderate Vertical Irregularity, V <sub>L1</sub> -0.7       -0.7       -0.6       -0.5       -0.5       -0.6       -0.4       -0.6       -0.5       -	Basic Score		3.6	3.2	2.9	2.1	2.0	2.6	-		1.5	2.0	_	1.6	1.4	1.7	1.7	1.0	
lan Irregularity, PL1       -1.1       -1.0       -0.0       -0.7       -0.6       -0.7       -0.7       -0.6       -0.5       0.0       -0.5       0.0       -0.5       0.0       0.0       -0.5       -0.6       0.0       0.0       0.0       -0.2       -0.3       -0.1       -0.1       -0.1       -0.1       -0.2       -0.4       0.5       0.6       0.0       0.0       -0.2       -0.3       0.1       -0.1       -0.1       -0.2       0.0       -0.2       0.3       0.1       -0.1       -0.2       0.0       -0.2       0.3       0.3       0.3       0.3       0.3       0.3       0.3       0.2       0.2       0.3       0.3       0.3<			1000		0.937500	13526	0.0283	10.53	33.32	-0.8		2022	1000	1936	11222	1.	-0.9		
re-Code       -1.1       -1.0       -0.9       -0.6       -0.6       -0.8       -0.6       -0.2       -0.4       -0.7       -0.1       -0.5       -0.3       -0.5       0.0         ost-Benchmark       1.6       1.9       2.2       1.4       1.4       1.1       1.9       NA       1.9       2.1       NA       2.0       2.4       2.1       2.1       NA       2.0       2.3       2.0       2.0       0.3       0.3       0.2       1.0.1       -0.5       0.6       0.5       0.5       0.3       0.3       0.3       0.2       1.		Ċ.	26.27		10000	2012/201	ST25532	266.00	0.000		0.0000000		63193	2020	10.000	10.000	1000	10.00	
ioil Type A or B       0.1       0.3       0.5       0.4       0.6       0.1       0.6       0.5       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.1       0.1       0.6       0.6       0.4       0.5       0.3       0.4       0.5       0.3       0.1       0.1       0.6       0.4       0.5       0.3       0.1       0.1       0.6       0.6       0.4       0.5       0.3       0.1       0.4       0.5       0.3       0.1       0.1       0.6       0.5       0.4       0.5       0.3       0.1       0.1       0.6       0.5       0.6       0.5       0.6       0.5       0.6       0.5       0.6       0.5       0.5       0.3       0.3       0.3       0.3       0.3       0.2       0.3       0.3       0.3       0.3       0.3       0.3       0.3       0.3       0.3 <td></td> <td></td> <td>1052.7</td> <td></td> <td></td> <td>10000085</td> <td>202220</td> <td></td> <td>12225</td> <td>10.665</td> <td></td> <td></td> <td></td> <td></td> <td>0000020</td> <td>10.000000</td> <td>12260</td> <td>25.252</td> <td></td>			1052.7			10000085	202220		12225	10.665					0000020	10.000000	12260	25.252	
oil Type E (1-3 stories)       0.2       0.2       0.1       -0.2       -0.4       0.2       -0.1       -0.4       0.0       0.0       -0.2       -0.3       -0.1       -0.1       -0.1       -0.2       -0.3       -0.6       -0.2       -0.3       -0.6       -0.2       -0.3       -0.4       -0.5       -0.7       -0.3       NA       -0.4       -0.5       -0.6       -0.2       -0.3       0.3       0.3       0.2       0.2       0.3       -0.6       -0.2       -0.3       -0.4       -0.5       -0.6       -0.2       -0.3       -0.4       -0.5       -0.5       -0.5       0.5       0.3       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.2       0.3					20230	100.00			0.656	1000	10.000	10000000	25753	1000	10000	300000	10002087	10000	1
Soli Type E (> 3 stories)       -0.3       -0.6       -0.9       -0.6       -0.6       NA       -0.6       -0.4       -0.5       -0.3       NA       -0.4       -0.5       -0.6       -0.2       -0.1         Minimum Score, Sumv       1.1       0.9       0.7       0.5       0.5       0.6       0.5       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.3 <td>지 않는 것 같아요. 이 것은 것을 잘 잘 했다. 또 한 것 같아요. 안 집에 집에 있는 것 같아요. 것 같아요. 것 같아요. 같아요. 같아요. 같아요. 같아요. 같아요. 같아요. 같아요.</td> <td></td> <td>072638</td> <td></td> <td>2618</td> <td>10000</td> <td>1122220</td> <td></td> <td>Section 2</td> <td>5022 and</td> <td>12.000.0003</td> <td>100 C</td> <td>2.250</td> <td></td> <td>1.532.53</td> <td></td> <td>100000</td> <td>10000</td> <td></td>	지 않는 것 같아요. 이 것은 것을 잘 잘 했다. 또 한 것 같아요. 안 집에 집에 있는 것 같아요. 것 같아요. 것 같아요. 같아요. 같아요. 같아요. 같아요. 같아요. 같아요. 같아요.		072638		2618	10000	1122220		Section 2	5022 and	12.000.0003	100 C	2.250		1.532.53		100000	10000	
INAL LEVEL 1 SCORE, SL1≥ SMM:       1.2         EXTENT OF REVIEW       OTHER HAZARDS         Action Required?       Partial         Interior:       Partial         Interior:       None         Interior:       None         Soil Type Source:       No         Beologic Hazards Source:       No         Beologic Hazards Source:       No         Geologic Hazards Source:       No         Beologic Hazards Source:       Pounding potential (unless St2>         Cut-off, if known)       Falling hazards from taller adjacent         Beologic Hazards Source:       Source:         EVEL 2 SCREENING PERFORMED?       Significant damage/deterioration to         Yes, Final Level 2 Score, St2       No         Nonstructural hazards?       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR         MR = Moment-resisting frame       RC = Reinforced concrete       URM INF = Unreinforced masonry infill       MH = Manufactured Housing FD = Flexible diaphrager	Soil Type E (> 3 stories)		-0.3	-0.6	-0.9	-0.6	-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6		
EXTENT OF REVIEW       OTHER HAZARDS         xterior:       Partial       All Sides       Aerial         terior:       None       Visible       Entered         petailed Structural Evaluation?       Pounding potential (unless Stars)       Pounding potential (unless Stars)         oil Type Source:       No       geotech report         ieologic Hazards Source:       Pounding potential (unless Stars)         Pounding back from taller adjacent       Withing         building       Geologic hazards or Soil Type F         Significant damage/deterioration to       Significant damage/deterioration to         the structural hazards?       Yes         Yes       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR       DNK	and a second	5 688	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3		0.3	0.2	0.2	0.3	0.3	0.2	
Are There Hazards That Trigger A tterior:       Partial       All Sides       Aerial         Are There Hazards That Trigger A terior:       None       Visible       Entered         interior:       No       Geotech report       Pounding potential (unless St2> cut-off, if known)       Ves. score less than cut-off         eologic Hazards Source:       No       geotech report       Pounding potential (unless St2> cut-off, if known)       Ves. score less than cut-off         eologic Hazards Source:       Opeotech report       Polialida Structural Evaluation Recommended? (check one)         EVEL 2 SCREENING PERFORMED?       Significant damage/deterioration to the structural system       No         Ves. Final Level 2 Score, Stap       No       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR         Where information cannot be verified, screener shall note the following:       MM INF = Unreliforced masonry infilm       MH = Manufactured Housing       FD = Flexible daphragm	INAL LEVEL 1 SCORE, S	L1 ≥ Smin:										1.2							
Interior:       None       Visible       Entered         Interior:       None       Visible       Entered         Interior:       No       Detailed Structural Evaluation?       Yes         Interior:       No       Detailed Nonstructural Evaluation Recommended? (check one)         Interior:       Significant damage/deterioration to the structural system       No         Detailed Nonstructural hazards       No       Detailed Nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary         Instructural hazards?       Yes       No       No       No         Where information cannot be verified	XTENT OF REVIEW																		
irrawings Reviewed:       Yes       No         oil Type Source:       No       geotech report         isolating hazards from taller adjacent building       Yes, sorte less than cut-off         isontact Person:       Falling hazards from taller adjacent building         isontact Person:       Geologic hazards or Soil Type F         isontact Person:       Significant damage/deterioration to the structural system         isontact Person:       No         Detailed Nonstructural hazards identified that should be evaluated to the structural system       No         isontructural hazards?       Yes         Yes       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR       DNK = Do Not Know         geged:       MR = Moment-resisting frame       RC = Reinforced concrete       URM INF = Unreinforced masonry infill       MH = Manufactured Housing       FD = Flexible diaphragm															2000 <b>-</b> 1200				
coil Type Source:       No geotech report         iselogic Hazards Source: No geotech report       cut-off, if known)         iselogic Hazards Source: No geotech report       Falling hazards from taller adjacent         building       Geologic hazards or Soil Type F         Significant damage/deterioration to the structural hazards?       No         Ves, Final Level 2 Score, St2       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR       DNK = D Not Know         Where information cannot be verified, screener shall note the following:       RC = Reinforced concrete       URM INF = Unreinforced masonry infill       MH = Manufactured Housing       FD = Flexible diaphragm	rawings Reviewed: 🔀 Yes		No .	-	200000					>						r other b	uilding		
Contact Person:       building         EVEL 2 SCREENING PERFORMED?       Geologic hazards or Soil Type F         Significant damage/deterioration to the structural hazards?       Significant damage/deterioration to the structural system       Detailed Nonstructural Hazards identified that should be evaluated         Non       No       No       No       Significant damage/deterioration to the structural system       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR       DNK         egend:       MR = Moment-resisting frame       RC = Reinforced concrete       URM INF = Unreinforced masonry infill       MH = Manufactured Housing       FD = Flexible diaphragm		<u> </u>			_	cut-o	off, if know	vn)			ΠY	es, other							
Constructural hazards identified that should be evaluated in the structural system     Constructural hazards identified that should be evaluated in the structural system     Constructural hazards?     Cons		<u>geote</u>	BCU LE	port	- 1			is from t	aller adja	cent			tructure	Evalua	tion Pr-	ommor	ded2 (al	ack one	1
Yes, Final Level 2 Score, St2        X       No       Instructural system       Instructural hazards exist that may require mitigation, but a detailed evaluation is not necessary         Jonstructural hazards?       X       Yes       X       No       <		DEDEC	OPME	<b>D</b> 2		Geo	logic haza				<u> </u>								
Ites, Final Level 2 scole, 02       Ites       Ites, Final Level 2 scole, 02       Ites       Ites<		gan sectores	JRIVIEI						elerioratio	n to	🗆 N	o, nonstri	uctural ha	azards e	xist that				
Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data         OR         DNK = Do Not Know           egend:         MRF = Moment-resisting frame         RC = Reinforced concrete         URM INF = Unreinforced masonry Infill         MH = Manufactured Housing         FD = Flexible diaphragm																ed li			
egend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry Infill MH = Manufactured Housing FD = Flexible diaphragm		5 333 a.	cannot b		880) L.	ner sha	ll note th	e follow	ving: ES	T = Esti	100000000000					1942	A Charles		
ык = ыraced trame SW = snear waii TU = Tilt up LM = Light metal RD = Rigid diaphragm	egend: MRF = I	Moment-resi	isting fram	e	RC = Rein	forced co			URM INF =	Unreinfo	2.25.152231		MH	= Manufa	ctured Ho	using F	D = Flexib		
	BR = Br	raced frame			SW = She	ar wall			i U = Tilt u	0			LM :	= Light me	etal	R	u = Rigid	diaphragn	n

### Barnette Elementary School: 1974 Addition

#### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

1000 Barnette Street Address: Zip: 99701 Fairbanks, Alaska Other Identifiers: Barnette Elementary School 1974 Addition **Building Name:** schoo Use: 64.8382 deg N Longitude: 147.7303 deg W Latitude: 0.992 0.378 Ss: S1: SMG February 2017 Date/Time: Screener(s): Year Built: 1974 D EST No. Stories: Above Grade: Below Grade: 0 .000 16 Code Year: 1970 Total Floor Area (sq. ft.): Additions: None X Yes, Year(s) Built: 1970, 1974 Emer. Services Historic Shelter Assembly Commercial Occupancy: Industrial Office School Government Utility Warehouse Residential, # Units: ПВ ПC ΠE □F DNK Soil Type: Soft If DNK, assume Type D. Hard Dense Poor Avg Rock Rock Soil Soil Soil Soil Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt.: Yes/No/DNK Pounding Falling Hazards from Taller Adjacent Building Adjacency: Vertical (type/severity) Irregularities: Plan (type) Reentrant corner Unbraced Chimneys Heavy Cladding or Heavy Veneer Exterior Falling Hazards: Parapets Appendages Other: COMMENTS: Addition forms reentrant corner where it connects to original building's shear wall for lateral and vertical support. SKETCH Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 S5 (URM INF) C3 (URM INF) FEMA BUILDING TYPE Do Not W1 W1A S1 (MRF) S2 (BR) \$3 (LM) \$4 (RC C1 (MRF PC1 (TU) PC2 RM1 (FD) RM2 URM MH Know (RD) **Basic Score** 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vertical Irregularity, VL1 -1.2 -1.2 -1.2 -1.0 -1.0 -1.1 -1.0 -0.8 -0.9 -1.0 -0.7 -1.0 -0.9 -0.9 -0.9 -0.7 NA Moderate Vertical Irregularity, VL1 -0.7 -0.7 -0.7 -0.6 -0.7 -0.6 -0.5 -0.5 -0.6 -0.4 -0.5 -0.5 -0.4 NA -0.6 -0.6 -0.5 Plan Irregularity, PL1 -1.1 -1.0 -1.0 -0.8 -0.7 -0.9 -0.7 -0.6 -0.6 -0.8 -0.5 -0.7 -0.6 -0.7 -0.7 -0.4 NA Pre-Code -1.1 -1.0 -0.9 -0.6 -0.6 -0.8 -0.6 -0.2 -0.4 -0.7 -0.1 -0.5 -0.3 -0.5 -0.5 0.0 -0.1 2.1 Post-Benchmark 1.6 2.2 1.4 1.9 NA NA 2.0 NA 1.2 1.9 1.4 1.1 1.9 2.1 2.4 2.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.5 0.3 0.3 Soil Type E (1-3 stories) 0.2 0.2 0.1 -0.2 -0.4 0.2 -0.1 -0.4 0.0 0.0 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2 -0.4 Soil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 -0.6 NA -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, SM 1.1 0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.3 0.2 0.2 0.3 0.3 0.2 1.0 1.9 1.2 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: OTHER HAZARDS ACTION REQUIRED EXTENT OF REVIEW 🔀 All Sides 🗌 Aerial Exterior: Partial Are There Hazards That Trigger A **Detailed Structural Evaluation Required?** Yes, unknown FEMA building type or other building Yes, score less than cut-off Visi Visible D Entered Detailed Structural Evaluation? Interior: None Interior: Drawings Reviewed: Yes No No geotech report Pounding potential (unless S<sub>12</sub> > cut-off, if known) Yes, other hazards present Geologic Hazards Source: No geotech report Falling hazards from taller adjacent No No Contact Person: building Detailed Nonstructural Evaluation Recommended? (check one) Geologic hazards or Soil Type F Yes, nonstructural hazards identified that should be evaluated LEVEL 2 SCREENING PERFORMED? Significant damage/deterioration to No, nonstructural hazards exist that may require mitigation, but a the structural system Yes, Final Level 2 Score, SL2 X No detailed evaluation is not necessary Nonstructural hazards? X No X Yes No. no nonstructural hazards identified X DNK Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know MRF = Moment-resisting frame BR = Braced frame MH = Manufactured Housing LM = Light metal RC = Reinforced concrete SW = Shear wall FD = Flexible diaphrag RD = Rigid diaphragm URM INF = Unreinforced masonry infill Legend TU = Tilt up Dennis L. Berry, PE Troy J. Feller, PE Colin Maynard, PE Scott M. Gruhn, PE **Greg Latreille, PE** 

Dennis L. Berry, PE

Troy J. Feller, PE

Hunter Elementary School: 1956 Original Construction

Geologic Hazards Source:N Contact Person: LEVEL 2 SCREENING Yes, Final Level 2 Score,	G PERFC	RME	D? X N X N			ficant da tructural		terioratio	n to	No de	o, nonstri tailed ev		azards e: s not ne	xist that i cessary	may requ	uld be ev uire mitig DNK	ation, bu	ta
Geologic Hazards Source:N Contact Person:	G PERFC	RME						terioratio	n to		o, nonstru	uctural ha	azards e	xist that i				ta
Geologic Hazards Source:		_								I V	ac nonet	nuctural h	azarde i	dentified	that aha		indicate d	
Geologic Hazards Source:	-		76		build		ards or S	oil Type	F							19.011.019	eck one)	
Soil Type Source: N					Fallin	g hazard		aller adja	cent			nazarus	present					
Drawings Reviewed: 🔀 Ye	s DN		eport		Pour	ding pot ff, if knov		less SL2	>	🗙 Ye	es, score	less than hazards	n cut-off	5 912 0				
nterior: 🐹 No	ne 🗌 V	/isible			Detailed				•	200		wn FEM				uilding		
EXTENT OF REVIEW Exterior:		Il Sidee	🗌 Aeri	al	OTHER Are Ther							EQUIF tural Eva		Require	d?			
FINAL LEVEL 1 SCORE, S								24										
Ainimum Score, SMW		1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1
Soil Type E (> 3 stories)		-0.3	-0.6	-0.9	-0.6	-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	M
ioil Type A or B ioil Type E (1-3 stories)		0.1 0.2	0.3 0.2	0.5	0.4 -0.2	0.6 -0.4	0.1 0.2	0.6 -0.1	0.5 -0.4	0.4	0.5 0.0	0.3 -0.2	0.6 -0.3	0.4 -0.1	0.5 -0.1	0.5 -0.1	0.3 -0.2	
ost-Benchmark		1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA 0.5	1.9	2.1	NA 0.3	2.0	2.4	2.1	2.1	NA 0.2	
re-Code		-1.1	-1.0	-0.9	-0.6	-0.6	-0.9	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	
oderate Vertical Irregularity, V <sub>L</sub> an Irregularity, P <sub>L1</sub>	1	-0.7 -1.1	-0.7 -1.0	-0.7 -1.0	-0.6	-0.6 -0.7	-0.7 -0.9	-0.6 -0.7	-0.5 -0.6	-0.5 -0.6	-0.6	-0.4 -0.5	-0.6 -0.7	-0.5 -0.6	-0.5 -0.7	-0.5 -0.7	-0.4 -0.4	
evere Vertical Irregularity, VL1		-1.2	-1.2	-1.2	-1.0	-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	
asic Score		3.6	3.2	2.9	2.1	2.0	2.6	SW) 2.0	INF)	1.5	2.0	INF)	1.6	1.4	1.7	1.7	1.0	
EMA BUILDING TYPE	Do Not Know	W1	W1A	W2	<b>S1</b> (MRF)	S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	
		В	ASIC	sco	RE, MO	DIFIE												
	SKE	тсн						Additiona	al sketch	es or cor	nments c	on separa	ite page					
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and the second division of the second divisio		_						gularitie	s:	100 <b>000</b> 000		pe/severi				. injaodi	. salutily	
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							Gan	logic H	Rock	Rock	Soi					Surf P	upt.: Yes/	No
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BBFM Engineers Rapid Visual Screening of Fairbanks North Star Borough Schools for Seismic Risk Page A6

Colin Maynard, PE

Scott M. Gruhn, PE

Greg Latreille, PE

## Hunter Elementary School: 1957 Addition

### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

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					42000		Occ	cupancy		embly Istrial ty	Comme Office Wareho		Emer. S School Residen	ervices tial, #Ur		istoric overnmer	Shel	ter
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FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2	(MRF)	<b>S2</b> (BR)	<b>S3</b> (LM)	\$4 (RC SW)	\$5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	M
Basic Score Severe Vertical Irregularity, VL1		3.6 -1.2	3.2 -1.2	2.9 -1.2	<b>2.1</b> -1.0	2.0 -1.0	2.6 -1.1	2.0 -1.0	1.7 -0.8	1.5 -0.9	-1.0	1.2 -0.7	1.6 -1.0	1.4 -0.9	-0.9	1.7 -0.9	1.0 -0.7	1. N
Moderate Vertical Irregularity, VL1		-0.7	-0.7	-0.7	-0.6	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	N
Plan Irregularity, PL1 Pre-Code		-1.1 -1.1	-1.0 -1.0	-1.0 -0.9	65 0.580.85	-0.7 -0.6	-0.9 -0.8	-0.7 -0.6	-0.6 -0.2	-0.6 -0.4	-0.8 -0.7	-0.5	-0.7 -0.5	-0.6 -0.3	-0.7 -0.5	-0.7	-0.4	N. -0
Post-Benchmark		1.6	1.9	2.2	201 812 X 20	1.4	-0.8	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.
Soil Type A or B		0.1	0.3	0.5	10000	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0
Soil Type E (1-3 stories) Soil Type E (> 3 stories)		0.2 -0.3	0.2 -0.6	0.1	-0.2	-0.4 -0.6	0.2 NA	-0.1 -0.6	-0.4 -0.4	0.0 -0.5	0.0 -0.7	-0.2 -0.3	-0.3 NA	-0.1 -0.4	-0.1 -0.5	-0.1 -0.6	-0.2 -0.2	-0 N
Minimum Score, S <sub>MW</sub>		-0.3	-0.8	-0.9	0.5	-0.6	0.6	-0.6	-0.4	-0.5	-0.7	0.3	0.2	-0.4	0.3	0.3	-0.2	1.
FINAL LEVEL 1 SCORE, SL	1 ≥ S <sub>MIN</sub> :										1.2				1.0			
EXTENT OF REVIEW					OTHE	R HAZ	ARDS	5		ACT	ION R	EQUIF	RED					
Exterior:  Parti	al 🔀 A	All Sides	Aer	ial	Are Ther				A		led Struc			Require	d?			
Interior: X None	e 🗆 ۱	/isible	Ent		Detailed					2012	es, unkn					uilding		
Drawings Reviewed: X Yes Soil Type Source: NC	geote		enort		Pour			nless SL2	>	XY	es, score	less that	n cut-off			3		
Geologic Hazards Source: No						ff, if knov ng hazaro		aller adia	cent		es, other	hazards	present					
Contact Person:					build	ing					led Nons	tructura	l Evalua	tion Rec	ommen	ded? (ch	eck one	
LEVEL 2 SCREENING	PEPEZ		D2			ogic haza ficant da					es, nonsi					1912		
Yes, Final Level 2 Score, S				0		ficant da tructural		sterioradio	01110	N	lo, nonstr	uctural h	azards e	xist that i				ta
	Yes						1997 (Par)				etailed ev lo, no nor				ed D			
Where info	all all sheet a	annot b			eener sha	ll note th	e follow	ving: E	ST = Est			-10 -11 - 11 - 12 <b>1</b> - 12		(ex-1+0,0,0%) S	100			
Legend: MRF = M	foment-resi	20.652.31.9	10	RC = R	einforced co			URM INF	= Unreinfo	S. 25. 1998		MH	= Manufa	ctured Ho	using F	D = Flexib	ile diaphra	gm
BR = Bra	aced frame			SW = S	hear wall			TU = Tilt u	qu			LM	= Light me	etal	R	D = Rigid	diaphragn	n
	_	roy J			_	0			DE		Scott							
ennis L. Berry, PE								vnard									atreil	

### Hunter Elementary School: 1958 Addition

#### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

1630 Gillam Way Address: Zip: 99701 Fairbanks, Alaska Other Identifiers Hunter Elementary School 1958 Addition **Building Name:** schoo Use: 64.8324 deg N 147.7311 deg W Latitude: Longitude: 0.994 0.379 Ss: S1: SMG February 201 Date/Time: Screener(s): Year Built: 1958 D EST No. Stories: Above Grade: Below Grade: C 7.000 Code Year:19 Total Floor Area (sq. ft.): Additions: 🗌 None X Yes, Year(s) Built: 1957. 1958, 1959, 1974 Historic Shelter Assembly Commercial Emer. Services Occupancy: Industrial Office Government School Utility Warehouse Residential, # Units: ПВ ПC DD □F DNK Soil Type: ΠE If DNK, assume Type D. Hard Dense Soft Poor Avg Rock Rock Soil Soil Soil Soil Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt.: Yes/No/DNK Pounding Falling Hazards from Taller Adjacent Building Adjacency: Vertical (type/severity) Irregularities: I Plan (type) Reentrant corner Unbraced Chimneys Heavy Cladding or Heavy Veneer Exterior Falling Hazards: Parapets Appendages Other: COMMENTS: Addition forms reentrant corner where the new wall frames over the top of the original building's shear wall for lateral and vertical support - and about 7' of it has a 1 1/2" vertical gap between the two walls for an expansion joint, with the new wall being supported by a 6x12 wood beam. Wood decking is the diaphragm. SKETCH Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 S5 (URM INF) C3 (URM INF) FEMA BUILDING TYPE Do Not W1 W1A W2 S1 (MRF) S2 (BR) \$3 (LM) \$4 (RC C1 (MRF C2 PC1 PC2 RM1 (FD) RM2 (RD) URM MH Know (SW) (TU) **Basic Score** 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vertical Irregularity, VL1 -1.2 -1.2 -1.2 -1.0 -1.0 -1.1 -1.0 -0.8 -0.9 -1.0 -0.7 -1.0 -0.9 -0.9 -0.9 -0.7 NA Moderate Vertical Irregularity, VL1 -0.7 -0.7 -0.7 -0.5 -0.6 -0.4 -0.5 -0.5 -0.4 NA -0.7 -0.6 -0.6 -0.6 -0.5 -0.6 -0.5 Plan Irregularity, PL1 -1.1 -1.0 -1.0 -0.8 -0.7 -0.9 -0.7 -0.6 -0.6 -0.8 -0.5 -0.7 -0.6 -0.7 -0.7 -0.4 NA Pre-Code -1.1 -1.0 -0.9 -0.6 -0.6 -0.8 -0.6 -0.2 -0.4 -0.7 -0.1 -0.5 -0.3 -0.5 -0.5 0.0 -0.1 Post-Benchmark 1.6 2.2 1.4 1.9 NA NA 2.0 2.1 NA 1.2 1.9 1.4 1.1 1.9 2.1 2.4 2.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.5 0.3 0.3 Soil Type E (1-3 stories) 0.2 0.2 0.1 -0.2 -0.4 0.2 -0.1 -0.4 0.0 0.0 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2 -0.4 Soil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 -0.6 NA -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, SM 1.1 0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.3 0.2 0.2 0.3 0.3 0.2 1.0 1.9 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: ACTION REQUIRED EXTENT OF REVIEW OTHER HAZARDS 🔀 All Sides 🗌 Aerial Exterior: Partial Are There Hazards That Trigger A **Detailed Structural Evaluation Required?** Yes, unknown FEMA building type or other building Yes, score less than cut-off Visi Visible D Entered Detailed Structural Evaluation? Interior: None Interior: Drawings Reviewed: X Yes No Self Type Source: No geotech report Pounding potential (unless S<sub>L2</sub> > cut-off, if known) Yes, other hazards present Geologic Hazards Source: No geotech report Falling hazards from taller adjacent No No Contact Person: building Detailed Nonstructural Evaluation Recommended? (check one) Geologic hazards or Soil Type F Yes, nonstructural hazards identified that should be evaluated LEVEL 2 SCREENING PERFORMED? Significant damage/deterioration to No, nonstructural hazards exist that may require mitigation, but a the structural system Yes, Final Level 2 Score, SL2 X No detailed evaluation is not necessary Nonstructural hazards? X No X Yes No. no nonstructural hazards identified X DNK Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know MRF = Moment-resisting frame MH = Manufactured Housing LM = Light metal RC = Reinforced concrete SW = Shear wall FD = Flexible diaphrag RD = Rigid diaphragm JRM INF = U reinforced masonry infill Legend BR = Braced frame TU = Tilt up Dennis L. Berry, PE Troy J. Feller, PE Colin Maynard, PE Scott M. Gruhn, PE **Greg Latreille, PE** 

## Hunter Elementary School: 1959 Addition

Rapid Visual Screening of Buildings for Potential Seismic Hazards	
FEMA P-154 Data Collection Form	

### Level 1 HIGH Seismicity

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Drawings no	t av	ailal	ole	but		No.	Stories:	Abov	e Grade	-		w Grade	Ser States	Yea	r Built:	1959 (	
				bui	•		al Floor . litions:	Area (so		12,0 Yes, Y		uilt:	1957.		e Year: 3, 195	1955 59, 19	74
appears to b							upancy		embly	Comme		Emer. S				Shelt	
construction	to 1	957	ao	aitic	on			Indu Utili	istrial ty	Office Wareho		School Residen	tial, #Ur		overnmer	nt	
			-	1	and a	Soil	Type:	□A Hard Rock	□ <b>B</b> Avg Rock	Den: Soi	se S	tiff S	oft P		NK DNK, ass	ume Type	D.
			-			Geo	logic Ha	azards:	Liquefac	tion: Yes	No/DN	Lands	lide: Yes	NoDNK	Surf. R	upt.: Yes/	NoDNK
				The local division of	_	Adja	acency:		D Po	ounding		Falling H	azards fr	om Taller	r Adjacen	it Building	
$\sim$		T.		0	-	Irreg	gularitie	s:		ertical (ty			t oor	nor			
M.		-				Eut	erior Fal	ling		an (type) nbraced					ding or H	leavy Ver	loor
							ards:	iiriy	_	arapets	Granney	19		oendages		icavy vci	1001
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	and a second				ad a	t	o orig	ginal	build	ling's	shea	ar wa	all for	later	ral ar	hd	
						V	ertic	al su	pport								
						5	South	end	is co	oncre	te be	aring	g/she	ear w	all; o	ther	
						V	valls	are v	vood	stud	bea	ring/s	shea	r wal	ls.		
							Nood										
						_											
	SKET						Additiona										
FEMA BUILDING TYPE	Do Not	BASI W1 W1		SI S1	S2	33 S3	ND FIN	S5	C1	C2	C3	L1 PC1	PC2	RM1	RM2	URM	МН
	Know			(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)	2/25/385 	(FD)	(RD)		1002000
Basic Score		3.6 3.2			2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1		-1.2 -1.:		100	-1.0 -0.6	-1.1 -0.7	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0 -0.6	-0.9 -0.5	-0.9	-0.9	-0.7 -0.4	NA NA
moderate venucar megularity, v2			-0		-0.0			0.5		0.6					0.5		
Plan Irregularity, Put		Sec. 10.00	-1.0	0 -0.8	-0.7		-0.6 -0.7	-0.5 -0.6	-0.5 -0.6	-0.6	-0.4 -0.5		10.000	-0.5 -0.7	-0.5 -0.7	10.00	
Plan Irregularity, PL1 Pre-Code	32	-0.7 -0. -1.1 -1.1 -1.1 -1.1		11000	-0.7 -0.6	-0.9 -0.8	-0.6 -0.7 -0.6	-0.5 -0.6 -0.2	-0.5 -0.6 -0.4	-0.6 -0.8 -0.7	-0.4 -0.5 -0.1	-0.7 -0.5	-0.5 -0.6 -0.3	-0.5 -0.7 -0.5	-0.5 -0.7 -0.5	-0.4 0.0	NA -0.1
Pre-Code Post-Benchmark		-1.1 -1.) -1.1 -1.) 1.6 1.9	-0.1	9 -0.6 2 1.4	-0.6 1.4	-0.9 -0.8 1.1	-0.7 -0.6 1.9	-0.6 -0.2 NA	-0.6 -0.4 1.9	-0.8 -0.7 2.1	-0.5 -0.1 NA	-0.7 -0.5 2.0	-0.6 -0.3 2.4	-0.7 -0.5 2.1	-0.7 -0.5 2.1	-0.4 0.0 NA	NA -0.1 1.2
Pre-Code Post-Benchmark Soil Type A or B	-	-1.1 -1.1 -1.1 -1.1 1.6 1.9 0.1 0.3	0 -0.1 2.2 0.5	9 -0.6 2 1.4 5 0.4	-0.6 1.4 0.6	-0.9 -0.8 1.1 0.1	-0.7 -0.6 1.9 0.6	-0.6 -0.2 NA 0.5	-0.6 -0.4 1.9 0.4	-0.8 -0.7 2.1 0.5	-0.5 -0.1 NA 0.3	-0.7 -0.5 2.0 0.6	-0.6 -0.3 2.4 0.4	-0.7 -0.5 2.1 0.5	-0.7 -0.5 2.1 0.5	-0.4 0.0 NA 0.3	NA -0.1 1.2 0.3
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories)	-	1.1     -1.1       -1.1     -1.1       1.6     1.5       0.1     0.3       0.2     0.2	0 -0.1	9 -0.6 2 1.4 5 0.4 -0.2	-0.6 1.4 0.6 -0.4	-0.9 -0.8 1.1 0.1 0.2	-0.7 -0.6 1.9 0.6 -0.1	-0.6 -0.2 NA 0.5 -0.4	-0.6 -0.4 1.9 0.4 0.0	-0.8 -0.7 2.1 0.5 0.0	-0.5 -0.1 NA 0.3 -0.2	-0.7 -0.5 2.0 0.6 -0.3	-0.6 -0.3 2.4 0.4 -0.1	-0.7 -0.5 2.1 0.5 -0.1	-0.7 -0.5 2.1 0.5 -0.1	-0.4 0.0 NA 0.3 -0.2	NA -0.1 1.2 0.3 -0.4
Pre-Code Post-Benchmark Soil Type A or B	-	-1.1 -1.1 -1.1 -1.1 1.6 1.9 0.1 0.3	0 -0.1 2.2 0.5 0.1 3 -0.1 0.7	9 -0.6 2 1.4 5 0.4 1 -0.2 9 -0.6 7 0.5	-0.6 1.4 0.6	-0.9 -0.8 1.1 0.1	-0.7 -0.6 1.9 0.6	-0.6 -0.2 NA 0.5	-0.6 -0.4 1.9 0.4	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3	-0.5 -0.1 NA 0.3	-0.7 -0.5 2.0 0.6	-0.6 -0.3 2.4 0.4	-0.7 -0.5 2.1 0.5	-0.7 -0.5 2.1 0.5	-0.4 0.0 NA 0.3	NA -0.1 1.2 0.3
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)		1.1     -1.1       -1.1     -1.1       1.6     1.5       0.1     0.3       0.2     0.2       -0.3     -0.1	0 -0.1 2.2 0.5 0.1 3 -0.1	9 -0.6 2 1.4 5 0.4 1 -0.2 9 -0.6 7 0.5	-0.6 1.4 0.6 -0.4 -0.6	-0.9 -0.8 1.1 0.1 0.2 NA	-0.7 -0.6 1.9 0.6 -0.1 -0.6	-0.6 -0.2 NA 0.5 -0.4 -0.4	-0.6 -0.4 1.9 0.4 0.0 -0.5	-0.8 -0.7 2.1 0.5 0.0 -0.7	-0.5 -0.1 NA 0.3 -0.2 -0.3	-0.7 -0.5 2.0 0.6 -0.3 NA	-0.6 -0.3 2.4 0.4 -0.1 -0.4	-0.7 -0.5 2.1 0.5 -0.1 -0.5	-0.7 -0.5 2.1 0.5 -0.1 -0.6	-0.4 0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN		1.1     -1.1       -1.1     -1.1       1.6     1.5       0.1     0.3       0.2     0.2       -0.3     -0.1	0 -0.1 2.2 0.5 0.1 3 -0.1 0.7	9 -0.6 2 1.4 5 0.4 1 -0.2 9 -0.6 7 0.5 9	-0.6 1.4 0.6 -0.4 -0.6	-0.9 -0.8 1.1 0.1 0.2 NA 0.6	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5	-0.6 -0.2 NA 0.5 -0.4 -0.4	-0.6 -0.4 1.9 0.4 0.0 -0.5 0.3	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2	-0.6 -0.3 2.4 0.4 -0.1 -0.4	-0.7 -0.5 2.1 0.5 -0.1 -0.5	-0.7 -0.5 2.1 0.5 -0.1 -0.6	-0.4 0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, State FINAL LEVEL 1 SCORE, SL12	- - - -	1.1     -1.1       -1.1     -1.1       1.6     1.5       0.1     0.3       0.2     0.2       -0.3     -0.1	0 -0.9 222 0.5 0.1 5 -0.9 0 0.7 1.1	9 -0.6 2 1.4 5 0.4 1 -0.2 9 -0.6 7 0.5 9 0THE	-0.6 1.4 0.6 -0.4 -0.6 0.5	-0.9 -0.8 1.1 0.1 0.2 NA 0.6	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.6 -0.4 1.9 0.4 0.0 -0.5 0.3	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 <b>1.2</b>	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2	-0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	-0.7 -0.5 2.1 0.5 -0.1 -0.6	-0.4 0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Pre-Code           Post-Benchmark           Soil Type A or B           Soil Type E (1-3 stories)           Soil Type E (> 3 stories)           Minimum Score, Staw           FINAL LEVEL 1 SCORE, SL12           EXTENT OF REVIEW           Exterior:         Partial           Interior:         X None	≥ Smin: All S Visi	-1.1     -1.1       -1.1     -1.1       1.6     1.5       0.1     0.3       0.2     0.2       0.3     -0.1       1.1     0.8	0 -0.1 2.2 0.5 0.1 0.7 1.9 Aerial	9 -0.6 2 1.4 5 0.4 1 -0.2 9 -0.6 7 0.5 9 OTHE Are The	-0.6 1.4 0.6 -0.4 -0.6 0.5	-0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.6 -0.4 1.9 0.4 0.0 -0.5 0.3	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 <b>1.2</b>	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2	-0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	-0.4 0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (-3 stories) Minimum Score, Skew FINAL LEVEL 1 SCORE, SL12 EXTENT OF REVIEW Exterior: Partial Interior: X None Drawings Reviewed: X Yes	≥ Smin: No No	-1.1     -1.1       -1.1     -1.1       1.6     1.9       0.1     0.3       0.2     0.2       0.3     -0.1       1.1     0.8	0 -0.9 2.2 0 0.5 1 0.1 5 -0.9 0 0.7 1 9 Aerial	9 -0.6 2 1.4 5 0.4 -0.2 9 -0.6 7 0.5 9 OTHE Are The Detailed □ Pou	-0.6 1.4 0.6 -0.4 -0.6 0.5 <b>R HAZ</b> . re Hazard <b>i Structur</b> nding pote	-0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS as That 1 al Evaluential (ur	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 <b>ACT</b> Detail	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION RI ed Struc es, unkno es, score	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev own FEM less tha	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation IA buildir n cut-off	-0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 Require	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	-0.4 0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S <sub>MAV</sub> FINAL LEVEL 1 SCORE, S <sub>L1</sub> 2 EXTENT OF REVIEW Exterior: Interior: Drawings Reviewed: Soil Type Source: No of Statement Score Statement Scor	≥ Smiw: Smiw: Visi Qeotec	1.1 -1.1 1.1 -1.1 1.6 1.9 0.1 0.3 0.2 0.2 0.2 0.3 -0.1 1.1 0.9 Sides ↓ / Sides ↓ / the repo	0 -0.9 2.2 0.5 0.1 0.1 0.7 1.1 Aerial Entered rt	9 -0.6 2 1.4 5 0.4 -0.2 9 -0.6 7 0.5 9 OTHE Are The Detailec □ Pou cut-	-0.6 1.4 0.6 -0.4 -0.6 0.5 <b>R HAZ</b> <b>R HAZ</b> <b>I Structur</b> nding pote off, if know	-0.9 -0.8 1.1 0.2 NA 0.6 ARDS as That 1 al Evaluential (ur m)	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A nation?	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 <b>ACT</b> Detail Ye X Ye Y	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION R ed Struc es, unkno es, score es, other	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev own FEM less tha	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation IA buildir n cut-off	-0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 Require	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	-0.4 0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (2-3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SL12 EXTENT OF REVIEW Exterior:  Partial Interior:  None Drawings Reviewed:  Yes	≥ Smiw: Smiw: Visi Qeotec	1.1 -1.1 1.1 -1.1 1.6 1.9 0.1 0.3 0.2 0.2 0.2 0.3 -0.1 1.1 0.9 Sides ↓ / Sides ↓ / the repo	0 -0.9 2.2 0.5 0.1 0.1 0.7 1.1 Aerial Entered rt	9 -0.6 2 1.4 5 0.4 -0.2 9 -0.6 7 0.5 9 OTHE Are The Detailec Pou cut- Fall	-0.6 1.4 0.6 -0.4 -0.6 0.5 <b>R HAZ</b> . re Hazard <b>i Structur</b> nding pote	-0.9 -0.8 1.1 0.2 NA 0.6 ARDS as That 1 al Evaluential (ur m)	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A nation?	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 <b>ACT</b> Detail Ye X Ye Ya Ya	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION R ed Struc es, unkno es, score es, other	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev own FEN less tha hazards	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation NA buildir n cut-off present	-0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 Require	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	-0.4 0.0 NA 0.3 -0.2 -0.2 0.2	NA -0.1 1.2 0.3 -0.4 NA 1.0
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SL12 EXTENT OF REVIEW Exterior: Interior: Partial Interior: Soil Type Source: O Geologic Hazards Source: Contact Person:	≥ Smin: ≥ Smin: No geotec geotec	1.1     -1.1       -1.1     -1.1       1.6     1.8       0.1     0.3       0.3     -0.1       1.1     0.3       ble     1       ble     1       chrepo     1.1	0 -0.9 2.2 0.5 0.1 0.1 0.7 1.1 Aerial Entered rt	9 -0.6 2 1.4 5 0.4 -0.2 9 -0.6 7 0.5 9 OTHE Are The Detailec Pou cut- Fall built U	-0.6 1.4 0.6 -0.4 -0.6 0.5 R HAZ. re Hazard I Structur: nding pote off, if know ing hazard ding Nogic haza	-0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That T al Evalue ential (ur vn) s from ta	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A hation? nless St2 aller adja	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 > cent	-0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 <b>ACT</b> Detail Y 4 X Y 4 Detail	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION R ed Struc es, unkno es, score es, other o	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev own FEM less tha hazards	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation IA buildir n cut-off present	-0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 Require	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	-0.4 0.0 NA 0.3 -0.2 -0.2 0.2	NA -0.1 1.2 0.3 -0.4 NA 1.0
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SL12 EXTENT OF REVIEW Exterior: Drawings Reviewed: Yes Soil Type Source: O Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING P	≥ Smin: Smi	1.1 -1.1 1.1 -1.1 1.1 -1.1 1.6 1.9 0.1 0.3 0.2 0.3 0.3 -0.1 1.1 0.9 Sides ↓ / ble ↓ F h repo h repo	0 -0.9 2.2 0.5 0.5 0.1 3 -0.9 0.7 1.1 Nerial Entered rt	9 -0.6 2 1.4 5 0.4 -0.2 9 -0.6 7 0.5 9 OTHE Are The Detailec Pou cut- Fall built Geee Sigr	-0.6 1.4 0.6 -0.4 -0.6 0.5 <b>R HAZ</b> <b>R HAZ</b> <b>R HAZ</b> <b>re Hazard</b> <b>I Structur</b> nding pote off, if know ing hazard ding logic hazard infocant dar	-0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That 1 al Evaluential (ur m) is from ta ards or S mage/de	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A hation? nless St2 aller adja	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 > cent	-0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 ACT Detail Y Ye No Detail	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION R ed Struc es, score ss, score o de Nonsi es, nonstr	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev wwn FEM less tha hazards tructural	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation IA buildir n cut-off present I Evalua hazards	-0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 Require ng type o	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ed? r other bits commented	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 uilding ded? (ch build be ev	-0.4 0.0 NA 0.3 -0.2 -0.2 0.2	NA -0.1 1.2 0.3 -0.4 NA 1.0
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SL12 EXTENT OF REVIEW Exterior: Partial Interior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: No Geologic Hazards Source: No Geologic Hazards Source: No Contact Person: LEVEL 2 SCREENING P Yes, Final Level 2 Score, SL2	≥ Smin: Smin: Smin: Solo Sector Perfor	1.1 -1.1 1.1 -1.1 1.6 1.5 0.1 0.3 0.2 0.2 0.3 -0.0 Sides ↓ / ble ↓ f th repo th repo RMED?	0 -0.9 2.2 0.5 0.5 0.1 0.1 0.7 0.7 1.9 No	9 -0.6 2 1.4 5 0.4 -0.2 9 -0.6 7 0.5 9 OTHE Are The Detailec Pou cut- Fall built Geee Sigr	-0.6 1.4 0.6 -0.4 -0.6 0.5 R HAZ. re Hazard I Structur: nding pote off, if know ing hazard ding Nogic haza	-0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That 1 al Evaluential (ur m) is from ta ards or S mage/de	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A hation? nless St2 aller adja	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 > cent	-0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 <b>ACT</b> Detail Ye Ye Ye N N Detail Detail N N Detail O N N Detail O C N N O	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION R ed Struc es, unkno es, score es, other o ed Nonsi es, nonstru- o, nonstru-	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev wwn FEM less tha hazards tructural luctural luctural l	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation IA buildir n cut-off present I Evalua hazards e is not ne	-0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 Require og type o tion Rec identified xist that cessary	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ed? r other bits comment that sho may requ	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 uilding ded? (ch build be ev uire mitig	-0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	NA -0.1 1.2 0.3 -0.4 NA 1.0
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (2-3 stories) Minimum Score, Statu FINAL LEVEL 1 SCORE, SLate EXTENT OF REVIEW Exterior: Partial Interior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: No Geologic Hazards Source: No Geologic Hazards Source: No Contact Person: LEVEL 2 SCREENING P Yes, Final Level 2 Score, SLate Nonstructural hazards? Yes Yes	≥ Smin: All s No geotec PERFOR //es	1.1 -1.1 1.1 -1.1 1.6 1.5 0.1 0.3 0.2 0.2 0.3 -0.0 5ides ↓ / ble ↓ f th repo th repo KMED?	0 -0.9 2.2 0.5 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	9         -0.6           2         1.4           5         0.4           -0.2         9           9         -0.6           7         0.5           9         OTHE           Are The Detailec           Detailec           Fall           built           Gete           Sign           the	-0.6 1.4 0.6 -0.4 -0.6 0.5 <b>R HAZ</b> , re Hazard 1 Structural 1 Structural structural structural	-0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That 1 is from ta ential (ur m) is from ta s from ta s from ta	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A nation? nless S <sub>L2</sub> aller adja soil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 <b>ACT</b> Detail Y ( X Y ( V Y ( Detail V O Detail V N U D V ( N V O D V O D V O D V O V O O O O O O O O	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION R ed Struc es, unkno es, score es, other o ed Nonsi es, nonstru- tailed ev. o, no non	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev wwn FEM less tha hazards tructural uctural h aluation	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation IA buildir n cut-off present I Evalua hazards azards e is not ne al hazard	-0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 Require og type o tion Rec identified xist that cessary s identifi	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 c.3 c.3 c.3 c.4 c.3 c.3 c.4 c.4 c.4 c.4 c.4 c.4 c.4 c.4 c.4 c.4	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 uilding ded? (ch build be ev uire mitig	-0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	NA -0.1 1.2 0.3 -0.4 NA 1.0
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (-2 s stories) Minimum Score, Statu FINAL LEVEL 1 SCORE, SL12 EXTENT OF REVIEW Exterior: Partial Interior: Contact Person: Contact Person: Constructural hazards? Yes Where inform	≥ Smin: No Sector PERFOR /es mation can	1.1     -1.1       1.1     -1.1       1.1     -1.1       1.1     -1.1       1.6     1.5       0.1     0.3       0.2     0.2       0.3     -0.1       1.1     0.5       Sides     J       ble     E       Ehrepo     E       Chromotope     E       Chromotope     E       Image: State of the set of the	0 -0.9 2.2 0 0.5 0 0.7 1.9 0 0.7 1.9 No No No	9         -0.6           2         1.4           5         0.4           -0.2         9           9         -0.6           7         0.5           9         OTHE           Are The         Detailec           Detailec         Pou           cut-         Fall           built         Gece           Sign         the	-0.6 1.4 0.6 -0.4 -0.6 0.5 <b>R HAZ</b> , re Hazard <b>B Structure</b> nding pole off, if know ing hazard ding loggic haza ificant dan structural s	-0.9 -0.8 1.1 0.2 NA 0.6 ARDS is That T al Evalu milal (ur m) is from ta urds or S mage/de	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A hation? allers S <sub>L2</sub> aller adja soil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 0.4 0.5 > > > ccent F n to	-0.6 -0.4 1.9 0.4 0.0 0.5 0.3 <b>ACT</b> Detail Y Y Y Y Y N Detail N Detail N Detail N N C N N C N S S S S S S S S S S S S S	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION RI ed Struc es, unkno es, score es, unkno es, score es, other o ed Nonsi es, nonsto o, nonstru o, nonstru o, nonstru o, nonstru o, nonstru o, nonstru	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev wwn FEM less tha hazards tructural a hazards tructural structural structural ble data	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation IA buildir n cut-off present I Evalua azards e is not ne al hazards 2 zards e is not ne	-0.6 -0.3 2.4 0.4 -0.4 -0.4 0.2 <b>Require</b> og type o tion Reco kist that cessary is identified xist that DNK = D	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 r other bind that sho may required that sho may required to Not Ki	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 uilding uilding ded? (ch ould be ev uire mitig. DNK	-0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	NA -0.1 1.2 0.3 -0.4 <u>NA</u> 1.0
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (2-3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SLATE EXTENT OF REVIEW Exterior: Partial Interior: Partial Interior: Ves Soil Type Source: O Geologic Hazards Source: Contact Person: Contact Person: Constructural hazards? Ves Final Level 2 Score, Sup Where inform	≥ Smin:	1.1     -1.1       1.1     -1.1       1.1     -1.1       1.1     -1.1       1.6     1.5       0.1     0.3       0.2     0.2       0.3     -0.1       1.1     0.5       Sides     J       ble     E       Ehrepo     E       Chromotope     E       Chromotope     E       Image: State of the set of the	0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0	9         -0.6           2         1.4           5         0.4           -0.2         9           9         -0.6           7         0.5           9         OTHE           Are The Detailec           Detailec           Fall           built           Gete           Sign           the	-0.6 1.4 0.6 -0.4 -0.6 0.5 <b>R HAZ</b> , re Hazard <b>B Structure</b> nding pole off, if know ing hazard ding loggic haza ificant dan structural s	-0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That 1 al Evalu ential (ur nn) is from ta system e follow	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A nation? nless S <sub>L2</sub> aller adja soil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.5 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7	-0.6 -0.4 1.9 0.4 0.0 0.5 0.3 <b>ACT</b> Detail Y Y Y Y Y N Detail N Detail N Detail N N C N N C N S S S S S S S S S S S S S	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION RI ed Struc es, unkno es, score es, unkno es, score es, other o ed Nonsi es, nonsto o, nonstru o, nonstru o, nonstru o, nonstru o, nonstru o, nonstru	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 <b>EQUIF</b> tural Ev tural Ev wwn FEN less tha hazards tructural h aluation Lctural h aluation MH	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation IA buildir n cut-off present I Evalua azards e is not ne al hazards 2 zards e is not ne	-0.6 -0.3 2.4 -0.1 -0.1 -0.4 0.2 Require ng type o tion Rec ddentified ddentified dtion Rec ddentified DDIK = D DDIK = D	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 commen- that sho may requ that sho may requ that sho may requ that sho may requ that sho may requ that sho cont for the sho co	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	-0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	NA -0.1 1.2 0.3 -0.4 <u>NA</u> 1.0
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (1-3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SL12 EXTENT OF REVIEW Exterior: Partial Interior: Partial Interior: Contact Person: Conta	≥ Smin:	1.1     -1.1       1.1     -1.1       1.1     -1.1       1.1     -1.1       1.6     1.5       0.1     0.3       0.2     0.2       0.3     -0.1       1.1     0.5       Sides     J       ble     E       Ehrepo     E       Chromotope     E       Chromotope     E       Image: State of the set of the	0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0		-0.6 1.4 0.6 -0.4 -0.6 0.5 <b>R HAZ</b> , re Hazard <b>B Structure</b> nding pole off, if know ing hazard ding loggic haza ificant dan structural s	-0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That 1 al Evalu ential (ur nn) is from ta system e follow	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A lation? nless S <sub>L2</sub> aller adja soil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7	-0.6 -0.4 1.9 0.4 0.0 0.5 0.3 <b>ACT</b> Detail Y Y Y Y Y N Detail N Detail N Detail N N C N N C N S S S S S S S S S S S S S	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION RI ed Struc es, unkno es, score es, unkno es, score es, other o ed Nonsi es, nonsto o, nonstru o, nonstru o, nonstru o, nonstru o, nonstru o, nonstru	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 <b>EQUIF</b> tural Ev tural Ev wwn FEN less tha hazards tructural h aluation Lctural h aluation MH	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation NA buildin n cut-off present I Evalua hazards l azards e is not nee is not nee	-0.6 -0.3 2.4 -0.1 -0.1 -0.4 0.2 Require ng type o tion Rec ddentified ddentified dtion Rec ddentified DDIK = D DDIK = D	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 commen- that sho may requ that sho may requ that sho may requ that sho may requ that sho may requ that sho cont for the sho co	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	-0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	NA -0.1 1.2 0.3 -0.4 <u>NA</u> 1.0
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (1-3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SL12 EXTENT OF REVIEW Exterior: Partial Interior: Partial Interior: Contact Person: Conta	≥ Smin:	1.1     -1.1       1.1     -1.1       1.1     -1.1       1.1     -1.1       1.6     1.5       0.1     0.3       0.2     0.2       0.3     -0.1       1.1     0.5       Sides     J       ble     E       Ehrepo     E       Chromotope     E       Chromotope     E       Image: State of the set of the	0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0		-0.6 1.4 0.6 -0.4 -0.6 0.5 <b>R HAZ</b> , re Hazard <b>B Structure</b> nding pole off, if know ing hazard ding loggic haza ificant dan structural s	-0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That 1 al Evalu ential (ur nn) is from ta system e follow	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A lation? nless S <sub>L2</sub> aller adja soil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7	-0.6 -0.4 1.9 0.4 0.0 0.5 0.3 <b>ACT</b> Detail Y Y Y Y Y N Detail N Detail N Detail N N C N N C N S S S S S S S S S S S S S	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION RI ed Struc es, unkno es, score es, unkno es, score es, other o ed Nonsi es, nonsto o, nonstru o, nonstru o, nonstru o, nonstru o, nonstru o, nonstru	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 <b>EQUIF</b> tural Ev tural Ev wwn FEN less tha hazards tructural h aluation Lctural h aluation MH	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation NA buildin n cut-off present I Evalua hazards l azards e is not nee is not nee	-0.6 -0.3 2.4 -0.1 -0.1 -0.4 0.2 Require ng type o tion Rec ddentified ddentified dtion Rec ddentified DDIK = D DDIK = D	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 commen- that sho may requ that sho may requ that sho may requ that sho may requ that sho may requ that sho cont for the sho co	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	-0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	NA -0.1 1.2 0.3 -0.4 <u>NA</u> 1.0
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (1-3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SL12 EXTENT OF REVIEW Exterior: Partial Interior: Partial Interior: Contact Person: Conta	≥ Smin:	1.1     -1.1       1.1     -1.1       1.1     -1.1       1.1     -1.1       1.6     1.5       0.1     0.3       0.2     0.2       0.3     -0.1       1.1     0.5       Sides     J       ble     E       Ehrepo     E       Chromotope     E       Chromotope     E       Image: State of the set of the	0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0		-0.6 1.4 0.6 -0.4 -0.6 0.5 <b>R HAZ</b> , re Hazard <b>B Structure</b> nding pole off, if know ing hazard ding loggic haza ificant dan structural s	-0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That 1 al Evalu ential (ur nn) is from ta system e follow	-0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A lation? nless S <sub>L2</sub> aller adja soil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7	-0.6 -0.4 1.9 0.4 0.0 0.5 0.3 <b>ACT</b> Detail Y Y Y Y Y N Detail N Detail N Detail N N C N N C N S S S S S S S S S S S S S	-0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 1.2 ION RI ed Struc es, unkno es, score es, unkno es, score es, other o ed Nonsi es, nonsto o, nonstru o, nonstru o, nonstru o, nonstru o, nonstru o, nonstru	-0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 <b>EQUIF</b> tural Ev Wwn FEN less tha hazards tructural h aluation Lctural h aluation MH	-0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation NA buildin n cut-off present I Evalua hazards l azards e is not nee is not nee	-0.6 -0.3 2.4 -0.1 -0.1 -0.4 0.2 Require ng type o tion Rec ddentified ddentified dtiot Rec ddentified dtiot Rec DDK = D DDK = DDK = DD	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 commen- that sho may requ that sho may requ that sho may requ that sho may requ that sho may requ that sho cont for the sho co	-0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	-0.4 0.0 NA 0.3 -0.2 -0.2 0.2 0.2	NA -0.1 1.2 0.3 -0.4 <u>NA</u> 1.0

#### Hunter Elementary School: 1974 Addition

#### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

1630 Gillam Way Address: Zip: 99701 Fairbanks, Alaska Other Identifiers Hunter Elementary School 1974 Addition £ **Building Name:** schoo Use: 64.8324 deg N 147.7311 deg W atitude: Longitude: 0.994 0.379 Ss: S1: SMG February 201 Date/Time: Screener(s): Year Built: 1974 🗆 EST No. Stories: Above Grade: Below Grade: C Code Year: 197 600 Total Floor Area (sq. ft.): Additions: 🗌 None X Yes, Year(s) Built: 1957 1958, 1959, 1974 Historic Shelter Assembly Commercial Emer. Services Occupancy: Industrial Office School Government Utility Warehouse Residential, # Units: ПВ C DD □F DNK Soil Type: ΠE If DNK, assume Type D. Hard Dense Soft Poor Avg Rock Rock Soil Soil Soil Soil Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt.: Yes/No/DNK Pounding Falling Hazards from Taller Adjacent Building Adjacency: Vertical (type/severity) Irregularities: I Plan (type) Reentrant corners Unbraced Chimneys Heavy Cladding or Heavy Veneer Exterior Falling Hazards: Parapets Appendages Other: COMMENTS: Addition is nested within earlier additions but separated from them with a 1/2" expansion joint at the foundation. A similar joint is shown on sheet G1 at the wood roof though without a dimension, and no lateral system for the steel frame is shown. Therefore, it is likely that this addition is tied to the 1958 and 1959 additions for lateral loads. SKETCH Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 S5 (URM INF) C3 (URM INF) FEMA BUILDING TYPE Do Not W1 W1A **S1** S2 (BR) \$3 (LM) \$4 (RC C1 (MRF C2 PC1 (TU) PC2 RM1 (FD) RM2 (RD) URM MH (MRF Know (SW) **Basic Score** 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vertical Irregularity, VL1 -1.2 -1.2 -1.2 -1.0 -1.0 -1.1 -1.0 -0.8 -0.9 -1.0 -0.7 -1.0 -0.9 -0.9 -0.9 -0.7 NA Moderate Vertical Irregularity, VL1 -0.7 -0.7 -0.7 -0.7 -0.5 -0.6 -0.4 -0.5 -0.5 -0.4 NA -0.6 -0.6 -0.6 -0.5 -0.6 -0.5 Plan Irregularity, PL1 -1.1 -1.0 -1.0 -0.8 -0.7 -0.9 -0.7 -0.6 -0.6 -0.8 -0.5 -0.7 -0.6 -0.7 -0.7 -0.4 NA Pre-Code -1.1 -1.0 -0.9 -0.6 -0.6 -0.8 -0.6 -0.2 -0.4 -0.7 -0.1 -0.5 -0.3 -0.5 -0.5 0.0 -0.1 2.1 Post-Benchmark 1.6 2.2 1.4 1.9 NA NA 2.0 NA 1.2 1.9 1.4 1.1 1.9 2.1 2.4 2.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.5 0.3 0.3 Soil Type E (1-3 stories) 0.2 0.2 0.1 -0.2 -0.4 0.2 -0.1 -0.4 0.0 0.0 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2 -0.4 Soil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 -0.6 NA -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, SM 1.1 0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.3 0.2 0.2 0.3 0.3 0.2 1.0 1.9 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: EXTENT OF REVIEW OTHER HAZARDS ACTION REQUIRED 🔀 All Sides 🗌 Aerial Exterior: Partial Are There Hazards That Trigger A **Detailed Structural Evaluation Required?** Yes, unknown FEMA building type or other building Yes, score less than cut-off Visi Visible D Entered Detailed Structural Evaluation? Interior: None No geotech report Drawings Reviewed: 🔀 Pounding potential (unless S<sub>L2</sub> > Soil Type Source: cut-off, if known) Yes, other hazards present Geologic Hazards Source: No geotech report Falling hazards from taller adjacent No No Contact Person: building Detailed Nonstructural Evaluation Recommended? (check one) Geologic hazards or Soil Type F Yes, nonstructural hazards identified that should be evaluated LEVEL 2 SCREENING PERFORMED? Significant damage/deterioration to No, nonstructural hazards exist that may require mitigation, but a the structural system Yes, Final Level 2 Score, SL2 X No detailed evaluation is not necessary Nonstructural hazards? X No X Yes No. no nonstructural hazards identified X DNK Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know MRF = Moment-resisting frame MH = Manufactured Housing LM = Light metal RC = Reinforced concrete SW = Shear wall FD = Flexible diaphrag RD = Rigid diaphragm JRM INF = U reinforced masonry infill Legend BR = Braced frame TU = Tilt up Dennis L. Berry, PE Troy J. Feller, PE Colin Maynard, PE Scott M. Gruhn, PE **Greg Latreille, PE** 

### Hutchison Career Center 1973 Original Construction

#### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

3750 Geist Road Address: Zip: 99709 Fairbanks, Alaska Other Identifiers Hutchison Career Center 1973 Original **Building Name:** schoo Use: 64.8502 deg N 147.8176 deg W Latitude: Longitude: 0.994 0.379 Ss: S1: SMG February 201 Date/Time: Screener(s): No. Stories: Above Grade: Below Grade: 0 Year Built: 1973 DEST 222 Total Floor Area (sq. ft.): Code Year: 1970 Additions: 🗌 None X Yes, Year(s) Built: 1975 Emer. Services Assembly Commercial Historic Shelter Occupancy: Industrial Office School Government Utility Warehouse Residential, # Units: ПВ ПC □F DNK Soil Type: ΠE Soft If DNK, assume Type D. Hard Dense Poor Avg Rock Rock Soil Soil Soil Soil Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt.: Yes/No/DNK Pounding Falling Hazards from Taller Adjacent Building Adjacency: Vertical (type/severity) Irregularities: X Plan (type) Reentrant corner Unbraced Chimneys Heavy Cladding or Heavy Veneer Exterior Falling Appendages Hazards: Parapets Other: COMMENTS: Drawings not available. SKETCH Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 C3 (URM INF) FEMA BUILDING TYPE Do Not W1 W1A W2 S1 (MRF) S2 (BR) \$3 (LM) S **S**5 C1 (MRF C2 PC1 (TU) PC2 RM1 (FD) RM2 URM MH (URM INF) (RC Know (SW) (RD) **Basic Score** 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vertical Irregularity, VL1 -1.2 -1.2 -1.2 -1.0 -1.0 -1.1 -1.0 -0.8 -0.9 -1.0 -0.7 -1.0 -0.9 -0.9 -0.9 -0.7 NA Moderate Vertical Irregularity, VL1 -0.7 -0.7 -0.7 -0.7 -0.5 -0.6 -0.4 -0.5 -0.4 NA -0.6 -0.6 -0.6 -0.5 -0.6 -0.5 -0.5 Plan Irregularity, PL1 -1.1 -1.0 -0.8 -0.7 -0.9 -0.7 -0.6 -0.6 -0.8 -0.5 -0.7 -0.6 -0.7 -0.4 NA -1.0 -0.7 Pre-Code -1.1 -1.0 -0.9 -0.6 -0.6 -0.8 -0.6 -0.2 -0.4 -0.7 -0.1 -0.5 -0.3 -0.5 -0.5 0.0 -0.1 Post-Benchmark 1.6 1.9 2.2 1.4 1.9 NA 1.9 NA 2.0 2.4 NA 1.2 1.4 1.1 2.1 2.1 2.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.5 0.3 0.3 Soil Type E (1-3 stories) 0.2 0.2 0.1 -0.2 -0.4 0.2 -0.1 -0.4 0.0 0.0 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2 -0.4 Soil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 -0.6 NA -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, SM 1.1 0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.3 0.2 0.2 0.3 0.3 0.2 1.0 1.0 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: EXTENT OF REVIEW OTHER HAZARDS ACTION REQUIRED All S X Partial All Sides 🗌 Aerial Are There Hazards That Trigger A **Detailed Structural Evaluation Required?** Exterior: Yes, unknown FEMA building type or other building Yes, score less than cut-off Visible Entered Detailed Structural Evaluation? Interior: None Interior: Drawings Reviewed: Yes No Self Type Source: No geotech report Pounding potential (unless S<sub>12</sub> > cut-off, if known) Yes, other hazards present Geologic Hazards Source: No geotech report No No Falling hazards from taller adjacent Contact Person: building Detailed Nonstructural Evaluation Recommended? (check one) Geologic hazards or Soil Type F Yes, nonstructural hazards identified that should be evaluated LEVEL 2 SCREENING PERFORMED? Significant damage/deterioration to No, nonstructural hazards exist that may require mitigation, but a the structural system Yes, Final Level 2 Score, SL2 X No detailed evaluation is not necessary X No Nonstructural hazards? X Yes No. no nonstructural hazards identified X DNK Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know MRF = Moment-resisting frame BR = Braced frame MH = Manufactured Housing LM = Light metal RC = Reinforced concrete SW = Shear wall FD = Flexible diaphrag RD = Rigid diaphragm JRM INF = Unreinforced masonry infill Legend TU = Tilt up Dennis L. Berry, PE Troy J. Feller, PE Colin Maynard, PE Scott M. Gruhn, PE **Greg Latreille, PE** 

### Hutchison Career Center 1975 Addition

### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

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FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2	S1 (MRF)	<b>S2</b> (BR)	<b>S3</b> (LM)	<b>\$4</b> (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score		3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1		-1.2	-1.2	-1.2	201 03550	-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Moderate Vertical Irregularity, V <sub>L</sub> ; Plan Irregularity, P <sub>L1</sub>	(	-0.7 -1.1	-0.7 -1.0	-0.7 -1.0	1000	-0.6 -0.7	-0.7 -0.9	-0.6 -0.7	-0.5 -0.6	-0.5 -0.6	-0.6 -0.8	-0.4 -0.5	-0.6 -0.7	-0.5 -0.6	-0.5	-0.5 -0.7	-0.4 -0.4	NA NA
Pian irregularity, PL1 Pre-Code		-1.1	-1.0	-1.0	1.	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	-0.1
Post-Benchmark		1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type A or B Soil Type E (1-3 stories)		0.1 0.2	0.3	0.5	0.4 -0.2	0.6 -0.4	0.1 0.2	0.6 -0.1	0.5 -0.4	0.4	0.5	0.3 -0.2	0.6 -0.3	0.4 -0.1	0.5 -0.1	0.5 -0.1	0.3 -0.2	0.3 -0.4
Soil Type E (> 3 stories)		-0.3	-0.6	-0.9		-0.4	NA	-0.1	-0.4	-0.5	-0.7	-0.2	-0.3 NA	-0.1	-0.1	-0.1	-0.2	-0.4 NA
Minimum Score, SMW		1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
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### Joy Elementary School 1971 Original Construction

#### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

24 Margaret Avenue Address: Fairbanks, Alaska 99701 Zip: Other Identifiers: Joy Elementary Center 1961 Original **Building Name:** schoo Use: 147.7251 deg W 64.8614 deg N atitude: Longitude: 0.987 0.376 Ss: S1: SMG February 201 Date/Time: Screener(s): No. Stories: Above Grade: Below Grade: 0 Year Built: 1961 D EST 222 Code Year: 1958 Total Floor Area (sq. ft.): Additions: X None Yes, Year(s) Built: Emer. Services Assembly Commercial Historic Shelter Occupancy: Industrial Office School Government Utility Warehouse Residential, # Units ПВ C D DNK Soil Type: ΠE **□**F If DNK, assume Type D. Hard Dense Soft Poor Avg Rock Rock Soil Soil Soil Soil Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt.: Yes/No/DNK Pounding Falling Hazards from Taller Adjacent Building Adjacency: Vertical (type/severity) Irregularities: X Plan (type) Reentrant corner X Unbraced Chimneys Heavy Cladding or Heavy Veneer Exterior Falling Appendages Hazards: Parapets Other: COMMENTS: Drawings not available. SKETCH Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 S5 (URM INF) C3 (URM INF) FEMA BUILDING TYPE Do Not W1 W1A W2 S1 (MRF) S2 (BR) \$3 (LM) \$4 (RC C1 (MRF PC1 (TU) PC2 RM1 (FD) RM2 (RD) URM MH Know **Basic Score** 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vertical Irregularity, VL1 -1.2 -1.2 -1.2 -1.0 -1.0 -1.1 -1.0 -0.8 -0.9 -1.0 -0.7 -1.0 -0.9 -0.9 -0.9 -0.7 NA Moderate Vertical Irregularity, VL1 -0.7 -0.7 -0.7 -0.6 -0.7 -0.6 -0.5 -0.5 -0.6 -0.4 -0.5 -0.5 -0.4 NA -0.6 -0.6 -0.5 Plan Irregularity, PL1 -1.1 -1.0 -1.0 -0.8 -0.7 -0.9 -0.7 -0.6 -0.6 -0.8 -0.5 -0.7 -0.6 -0.7 -0.7 -0.4 NA Pre-Code -1.1 -1.0 -0.9 -0.6 -0.6 -0.8 -0.6 -0.2 -0.4 -0.7 -0.1 -0.5 -0.3 -0.5 -0.5 0.0 -0.1 Post-Benchmark 1.6 1.9 2.2 1.4 1.9 NA 2.1 NA 2.0 2.1 NA 1.2 1.4 1.1 1.9 2.4 2.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.5 0.3 0.3 Soil Type E (1-3 stories) 0.2 0.2 0.1 -0.2 -0.4 0.2 -0.1 -0.4 0.0 0.0 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2 -0.4 Soil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 -0.6 NA -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, SM 1.1 0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.3 0.2 0.2 0.3 0.3 0.2 1.0 1.2 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN ACTION REQUIRED EXTENT OF REVIEW **OTHER HAZARDS** Exterior: Partial All Sides 🗌 Aerial Are There Hazards That Trigger A **Detailed Structural Evaluation Required?** Yes, unknown FEMA building type or other building Yes, score less than out off Visi Visible Entered Detailed Structural Evaluation? Interior: None Interior: Drawings Reviewed: Yes No Self Type Source: No geotech report Pounding potential (unless S<sub>12</sub> > cut-off, if known) Yes, other hazards present Geologic Hazards Source: No geotech report Falling hazards from taller adjacent No No Contact Person: building Detailed Nonstructural Evaluation Recommended? (check one) Geologic hazards or Soil Type F Yes, nonstructural hazards identified that should be evaluated LEVEL 2 SCREENING PERFORMED? Significant damage/deterioration to No, nonstructural hazards exist that may require mitigation, but a the structural system Yes, Final Level 2 Score, SL2 X No detailed evaluation is not necessary Nonstructural hazards? X No X Yes No. no nonstructural hazards identified X DNK Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know MRF = Moment-resisting frame BR = Braced frame MH = Manufactured Housing LM = Light metal RC = Reinforced concret SW = Shear wall FD = Flexible diaphrag RD = Rigid diaphragm JRM INF = U reinforced masonry infil Legend TU = Tilt up Dennis L. Berry, PE Troy J. Feller, PE Colin Maynard, PE Scott M. Gruhn, PE **Greg Latreille, PE** 

## Lathrop High School 1953 Original Construction

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FEMA BUILDING TYPE	Do Not Know	W1 W1/	W	2 <b>S1</b> (MRF)	<b>S2</b> (BR)	S3 (LM)	<b>S4</b> (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	мн
Basic Score		3.6 3.2	2.9	2.1	2.0	2.6	SW) 2.0	INF) 1.7	1.5	2.0	INF) 1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1		1.2 -1.2	1000	Sec. 245	-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Moderate Vertical Irregularity, VL1		0.7 -0.7		100000	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Plan Irregularity, PL1		1.1 -1.0		Set: 187856855	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Pre-Code Post-Benchmark		1.1 -1.0 1.6 1.9		3401 8823234	-0.6 1.4	-0.8 1.1	-0.6 1.9	-0.2 NA	-0.4 1.9	-0.7 2.1	-0.1 NA	-0.5 2.0	-0.3 2.4	-0.5 2.1	-0.5 2.1	0.0 NA	-0.1 1.2
Soil Type A or B		0.1 0.3	2,633	100.00	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories)		0.2 0.2	33535	1	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Soil Type E (> 3 stories)		0.3 -0.6	_		-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, SMN	44239	r.1 U.S	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1	$\geq SMIN$									1.2				1.0			
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Exterior:  Partial Interior:  None	X All S	Sides 🗌 A ble 🔲 E		Are The Detailed	Structur	al Evalu	ation?		□ Y	es, unkno	wn FEM	A buildir	ng type o	r other b	uilding		
Exterior:  Partial Interior:  None Drawings Reviewed:  Yes	X All S	ble 🔲 E	ntered	Are The Detailed	Structur nding pote	al Evalu ential (ur	ation?		Y X Y	es, unkno es, score	wn FEM less tha	IA buildir n cut-off	ng type o		uilding		
Exterior: Partial Interior: None Drawings Reviewed: Yes	X All S Visi X No geotec	ble 🔲 E	ntered t	Are The Detailed	Structur nding pote	al Evalu ential (ur vn)	nless SL2	>	V X Y	es, unkno es, score es, other	wn FEM less tha	IA buildir n cut-off	ng type o		uilding		
Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: No	X All S Visi X No geotec	ble 🔲 E	ntered t	Are The Detailed Pour cut-c Falli build	Structur nding pote off, if know ng hazard ling	al Evalu ential (ur vn) is from t	iation? nless S <sub>L2</sub> aller adja	> icent	Y Y Y Y	es, unkno es, score es, other o	own FEM less tha hazards	A buildir n cut-off present	ng type o			eck one)	
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## Lathrop High School 1957 Addition

### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

Know         (MRF)         (BR)         (LM)         (RC)         (URM)         (MRF)         (SW)         (URA)         (TU)         (FD)         (RD)           Basic Score         3.6         3.2         2.9         2.1         2.0         2.6         2.0         1.7         1.5         2.0         1.2         1.6         1.4         1.7         1.0         1	20			2			12	Add	lress:			rport				222	10.0		
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Use:         School         147.7328 deg           1.339         Str.         0.373           School         DataTine:         February 2017           School         DataTine:         February 2017           School         Str.         Octowership         DataTine:           School         School         Str.         Octowership           School         School         Str.         Octowership         Octowership           School         School         School         School         Octowership         Octowership           School	BAN BANS										athre	n Hic	h Car		OF7	Addit	on		
Latitude:       64.8362.0eg N       Longitude:       147.7328.deg         Sciencer(s):       Subsciencer(s):       DuteTime:       CeDurary 2017         No. Stofes:       Abore Grade:       Betworderde       Year Bull:       1952.         Additions:       No. Stofes:       Abore Grade:       Betworderde       Year Bull:       1957.         No. Stofes:       Abore Grade:       Betworderde       Betworderde       Year Bull:       1957.         Additions:       No. Stofes:       Abore Grade:       Betworderde       Year Bull:       1957.         Additions:       No. Stofes:       No. Stofes:       Betworderde       Year Bull:       1957.         Additions:       No. Stofes:       No. Stofes:       Betworderde       Year Bull:       1957.         Stofes:       Abore Grade:       Year Bull:       1957.       164.000000000000000000000000000000000000	A CARLES	1					-	64	-		_		n Scr	1001	957 1	Additi	on		
Sr:       0.993       Sr:       0.979         Scr:       Std:	and the state of t	UTILLUM	L F										N	ongitu	de.	14	7.73	28 de	a V
Second register         SMG         Data Time:         February 2017           No. Stories:         Abore Grade:         2         Below Grade:         7         Code Verait         1357.1           No. Stories:         No. Grade:         1         2.00         Code Verait         1377.1         1362.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         1377.1         137	A CONTRACTOR	State /		File-		-		3.4	uue.						ue				9.
Total Floor Area (sp. R):       12,000       Code Year 1955         Code Year 1955         Occupancy: Assently: Commercial Ener. Service: I Historic I Sheller         Index Floor Area (sp. R):       12,000       Code Year 1955         Occupancy: Assently: Commercial Ener. Service: I Historic I Sheller         Index Floor Area (sp. R):       12,000         Occupancy: Assently: Commercial Ener. Service: I Historic I Sheller         Set Type: I A B B Drac B St. Port       NMK essent Part         Set Type: I A B B Drac B St. Port       NMK essent Part         Occupancy: Assently: Commercial Ener. Service: I Historic I Sheller         Occupancy: Assently: Conding C Flag       NMK essent Part         Occupancy: Assently: Conding C Flag       NMK essent Part         Occupancy: Assently: Conding C Flag	Az A ALE		1	- ALA		3-4			eener(s)	: S	MG		8		ate/Time	e: F	ebrua	ary 20	17
Additional       Additional       Yes, Yes, Yes, Yes, Yes, Yes, Yes, Yes,			-	1 A	-			No.	Stories	: Abov	e Grade	e: 2	Belov	w Grade	: 0	Year	Built:	957	ES
Industrial         Office         Image: Comparison of the comment of						-								uilt:	1957,				_
Soil Type: _A _B _C				8		and the second		Occ	upancy	Indu	strial	Office		School		G			ler
Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Sketch       Concrete roof slab sits on haunch off concrete wall         Sketch       Sketch       Sketc								Soil	Туре:	<b>□A</b> Hard	□B Avg	Den	se St	D C	]E [ koft P	F D		ите Туре	D.
Adjacency:       Pounding       Faling Hazards from Taller Adjacent Building         Image: Second Sec			_			_		Geo	logic H								Surf R	int : Yes/	No
Image: Step in the second state in					-			-											
Image: Second State Second State S			-	-		-		_				ertical (ty							N <sub>1</sub> nccs
Hazards:       □			+		-	-					🔀 P	lan (type)	Ree	ntrar	nt cor	rner			
COMMENTS:         Concrete roof slab sits on haunch off concrete wall or existing concrete wall.           SKETCH			-		_					lling	🗆 P	arapets	Chimney	ſS				eavy Ver	neer
SKETCH         Additional sketches or comments on separate page           SKETCH						_		CO	MMENT	S:		ulti							
Additional sketches or comments on separate page         SKETCH         BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, S,r         FeMA BUILDING TYPE       Do Noti       With With       W2       \$\$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$						-		C	oncr	ete r	oof s	lab s	its or	hau	unch	off co	oncre	te w	all
BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, S <sub>L1</sub> FEMA BUILDING TYPE         Do Not Know         W1         W2         S1         S2         S3         S4         URM         MPF			-					0	r exis	sting	cond	crete	wall.						
BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, S <sub>L1</sub> FEMA BUILDING TYPE         Do Not Know         W1         W2         S1         S2         S3         S4         URM         MPF			-																
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BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, S <sub>L1</sub> FEMA BUILDING TYPE         Do Not Know         W1         W2         S1         S2         S3         S4         URM         MPF		eve	тен	in er		1			Addition	al al atab									
FEMA BUILDING TYPE         Do Not Know         W1         W1         W2         S1         S2         S3         S4         S5         C1         C2         C3         PC1         PC2         RM1         RM2         URM         N           Basic Score         3.6         3.2         2.9         2.1         2.0         2.6         2.0         1.7         1.5         2.0         1.2         1.6         1.4         1.7         1.7         1.0         0.9         0.0         0.7         0.7         0.7         0.6         0.6         0.6         0.6         0.6         0.6         0.6         0.6         0.6         0.6         0.4         0.5         0.3         0.5         0.4         0.5         0.4         0.5         0.4         0.5         0.4         0.5         0.4         0.5         0.4         0.5         0.4         0.5         0.4         0.5         0.4         0.5		JAL		ASIC	sco	RE MO	DIFIER												
Basic Score       3.6       3.2       2.9       2.1       2.0       2.6       2.0       1.7       1.5       2.0       1.2       1.6       1.4       1.7       1.7       1.0       1         Severe Vertical Irregularity, V_17       -0.7       -0.7       -0.7       -0.7       -0.6       -0.6       -0.5       -0.5       -0.6       -0.4       -0.6       -0.5       -0.5       -0.6       -0.4       -0.6       -0.5       -0.6       -0.6       -0.7       -0.6       -0.6       -0.7       -0.6       -0.6       -0.5       -0.6       -0.6       -0.5       -0.6       -0.6       -0.5       -0.6       -0.6       -0.6       -0.5       -0.6       <	FEMA BUILDING TYPE			Second read		S1	S2	\$3	<b>S4</b> (RC	S5 (URM	C1	C2	C3 (URM	PC1	PC2			URM	м
Moderate Vertical Irregularity, V <sub>1</sub> ;       -0.7       -0.7       -0.7       -0.6       -0.6       -0.5       -0.5       -0.6       -0.5       -0.6       -0.6       -0.6       -0.6       -0.6       -0.6       -0.6       -0.6       -0.6       -0.6       -0.6       -0.6       -0.6       -0.5       -0.5       -0.5       0.5       0.5       0.5       0.5       0.5       0.5       0.5       0.5       0.5       0.5       0.5       0.5       0.5       0.5	Basic Score		3.6	3.2	2.9	2.1	2.0	2.6			1.5	2.0		1.6	1.4	1.7	1.7	1.0	1
Plan Irregularity, PL:       -1.1       -1.0       -0.8       -0.7       -0.9       -0.7       -0.6       -0.6       -0.8       -0.7       -0.1       -0.5       -0.3       -0.5       -0.7       -0.6       -0.6       -0.8       -0.6       -0.6       -0.8       -0.6       -0.4       -0.5       -0.7       -0.6       -0.6       -0.6       -0.4       -0.5       -0.7       -0.3       -0.6       -0.6       -0.6       -0.4       -0.5       -0.7       -0.3       NA       -0.6 <td< td=""><td>Severe Vertical Irregularity, VL1</td><td></td><td>10000</td><td>62336</td><td>1.5.5</td><td>10.00</td><td>11.252</td><td></td><td>26.32</td><td>0.2222-0-0</td><td></td><td>2022</td><td>10000</td><td>1836</td><td>102200</td><td>1.</td><td>100.00</td><td></td><td>N</td></td<>	Severe Vertical Irregularity, VL1		10000	62336	1.5.5	10.00	11.252		26.32	0.2222-0-0		2022	10000	1836	102200	1.	100.00		N
Pre-Code       -1.1       -1.0       -0.9       -0.6       -0.6       -0.8       -0.6       -0.2       -0.4       -0.7       -0.1       -0.5       -0.3       -0.5       -0.5       0.0       -4         Post-Benchmark       1.6       1.9       2.2       1.4       1.4       1.1       1.9       NA       1.9       2.1       NA       2.0       2.4       2.1       2.4       2.1       2.4       2.1       2.4       2.1       2.4       2.1       2.4       2.1       2.4       2.1       2.4       2.1       2.4       2.1       2.4       2.1       1.4       1.4       1.1       1.9       NA       1.9       2.1       NA       2.0       2.4       2.1       2.4       2.1       2.4       2.1       2.1       NA       1.0       2.0       2.4       2.0       2.4       2.0       2.4       2.0       2.4       2.0       2.4       2.0       2.4       2.0       2.4       2.0       2.4       2.0       2.4       2.0       2.4       2.0       2.4       2.0       2.4       2.0       2.4       2.1       NA       4.4       2.0       2.4       2.1       NA       4.0       2.5			256.23	10,000	1000	1000	0.025532		0.555				6239	2022	10.000		53035	10.00	
Soil Type A or B       0.1       0.3       0.5       0.4       0.6       0.1       0.6       0.5       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.6       0.4       0.5       0.3       0.4       0.5       0.5       0.6       0.6       0.4       0.5       0.3       0.0       0.0       0.2       0.3       0.3       0.2       0.6       0.5       0.6       0.5       0.5       0.3       0.6       0.5       0.5       0.3       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.5       0.6       0.5       0.5       0.5       0.3       0.6       0.5       0.5       0.5       0.5 <td>Pre-Code</td> <td></td> <td>100000</td> <td>1000</td> <td>-0.9</td> <td>-0.6</td> <td>1000000</td> <td></td> <td>10.000</td> <td>0.5 372</td> <td></td> <td>-0.7</td> <td></td> <td></td> <td>2,222,227</td> <td>-0.5</td> <td>10.000</td> <td>19333</td> <td>-4</td>	Pre-Code		100000	1000	-0.9	-0.6	1000000		10.000	0.5 372		-0.7			2,222,227	-0.5	10.000	19333	-4
Soil Type E (1-3 stories)       0.2       0.2       0.1       -0.2       -0.4       0.2       -0.1       -0.4       0.0       0.0       -0.2       -0.3       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.1       -0.2       -1       1       1       0.9       -0.6       -0.6       NA       -0.6       -0.4       -0.5       -0.7       -0.3       NA       -0.4       -0.5       -0.6       -0.2       1       1       0.9       0.7       0.5       0.5       0.5       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2				0.525	10238	1000	1.		0.000	20322	10.000	242200	25522	1993	0.000	300000	- 303372382	10000	
Soil Type E (> 3 stories)       -0.3       -0.6       -0.9       -0.6       -0.6       NA       -0.6       -0.7       -0.3       NA       -0.4       -0.5       -0.7       -0.3       NA       -0.4       -0.5       -0.6       -0.2       N         Minimum Score, Sum       1.1       0.9       0.7       0.5       0.5       0.6       0.5       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.3       0.2       0.2       0.3       0.3       0.3       0.3       0.3       0.2       0.2       NA       -0.6       -0.6       0.2       NA       -0.6       -0.5       0.3       0.3       0.3       0.2       0.3       0.3       0.3       0.3       0.3       0.2       0.2	이 같은 것 이 가지 않는 것 같은 것 같		10000	2002	1018	10000	1000000		6.02	10000	500004	200303			180265		- C0223	1000	1.1
FINAL LEVEL 1 SCORE, S <sub>L1</sub> ≥ SMMX:       1.2       1.0         EXTENT OF REVIEW       OTHER HAZARDS       Action REQUIRED         Exterior:       Partial       All Sides       Aerial         Interior:       None       Visible       Entered         Drawings Reviewed:       Yes       No       Detailed Structural Evaluation?       Pounding potential (unless St2> cut-off, if known)       Pounding potential (unless St2> cut-off, if known)       Yes, score less than cut-off       Yes, score less than cut-off       Yes, other hazards present         Exterior:       Pounding potential (unless St2> cut-off, if known)       Falling hazards from taller adjacent building       No       Yes, other hazards present       No         Exterior:       Significant damage/deterioration to the structural system       Significant damage/deterioration to the structural system       No         Ves, Final Level 2 Score, St2       No       No       No       No, nonstructural hazards identified that should be evaluated dataide evaluation is not necessary       No, no nonstructural hazards identified to DNK         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data <u>OR</u> DNK = D Not Know         Where information fame       RC = Reinforced concrete       URM INF = Urreinforced masonry infil       MH = Manufactured Housing       PO = Flexible daphraam	Soil Type E (> 3 stories)					_	_					_			_				_
EXTENT OF REVIEW       OTHER HAZARDS         Exterior:       Partial       All Sides       Aerial         Interior:       None       Visible       Entered         Drawings Reviewed:       Yes       No         Soil Type Source:       No geotech report         Soil Type Source:       Pounding potential (unless S <sub>L2</sub> >         Cut-off, if known)       Falling hazards from taller adjacent         Beologic Hazards Source:       Performation cannot be verified, screener shall note the following:       EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know			1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	-	0.3	0.2	0.2		0.3	0.2	1
Exterior:       Partial       All Sides       Aerial         Interior:       None       Visible       Entered         Drawings Reviewed:       None       Visible       Entered         Soil Type Source:       No       Geotech report       Pounding potential (unless St2> cut-off, if known)       Yes, score less than cut-off         Soil Type Source:       No       geotech report       Pounding potential (unless St2> cut-off, if known)       Yes, other hazards present         Sololate Person:       Geotogic hazards from taller adjacent building       Geologic hazards or Soil Type F       Significant damage/deterioration to the structural system       No         Ves, Final Level 2 Score, St2       Mo       No       No       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data OR DNK = Do Not Know         Where information farme       RC = Reinforced concrete       URM INF = Urreinforced masonry infil       MH = Manufactured Housing       Pol = Fexible daphraam		L1 2 SMIN:			- 1				2.5		1000000000					1.0			
Interior:       None       Visible       Entered         Drawings Reviewed:       Ves       No       Detailed Structural Evaluation?       Yes, unknown FEMA building type or other building         Drawings Reviewed:       Ves       No       Pounding potential (unless St2> cut-off, if known)       Yes, score less than cut-off         Seologic Hazards Source:       No       Geotech report       Falling hazards from taller adjacent building       Yes, other hazards present         Contact Person:       Falling hazards or Soil Type F       Significant damage/deterioration to the structural system       Detailed Nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary         Nonstructural hazards?       Yes       No         Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know         Ware information fame         URM INF = Unreinforced masonry infil				<b>—</b> ••												10			
Drawings Reviewed:       Yes       No         Drawings Reviewed:       Yes       No         Sold Type Source:       No       Geologic Hazards from taller adjacent building         Seologic Hazards Source:No       Geologic hazards from taller adjacent building       No         Detailed Person:       Geologic hazards or Soil Type F       Significant damage/deterioration to the structural system       No         EVEL 2 SCREENING PERFORMED?       No       Yes, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary         Yes, Structural system       No       No nonstructural hazards identified       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know										4	1000								
Soil Type Source:       NO Geolecn report         Geologic Hazards Source: No geotech report       cut-off, if known)         Geologic Hazards Source: No geotech report       cut-off, if known)         Falling hazards from taller adjacent building       No         Detailed Nonstructural Evaluation Recommended? (check one)       Significant damage/deterioration to the structural system         Yes, Final Level 2 Score, Structural Nazards?       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know         Where information frame       RC = Reinforced concrete       URM INF = Unreinforced masonry infil       MH = Manufactured Housing       PE = Fexible diaphraam	Drawings Reviewed: 🔀 Yes		lo							>						or other bi	uliding		
Contact Person:       building         LEVEL 2 SCREENING PERFORMED?       Geologic hazards or Soil Type F         Significant damage/deterioration to the structural system       Ves. nonstructural hazards identified that should be evaluated         No.       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR NoK         Where information farme       RC = Reinforced concrete       URM INF = Unreinforced masonry infil       MH = Manufactured Housing       FD = Fexible diaphraam						cut-o	ff, if know	/n)			□ Y	es, other							
EVEL 2 SCREENING PERFORMED?     Geologic hazards or Soil Type F     Significant damage/deterioration to     the structural system     Ves, Final Level 2 Score, S <sub>L2</sub> X No     Nonstructural hazards?     Yes X No     Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know     Where information frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing - PD = Flexible diaphragm		geote	ech re	port				s from t	aller adja	icent									1
Yes, Final Level 2 Score, St2			_			Geol	ogic haza				1.						S	1002.000 <b>1</b>	ŝ
Yes, Final Level 2 Score, SL2     Active 2 Score,			RME		, 1				eterioratio	on to									ta
Where information cannot be verified, screener shall note the following:         EST = Estimated or unreliable data         OR         DNK = Do Not Know           egend:         MRF = Moment-resisting frame         RC = Reinforced concrete         URM INF = Unreinforced masonry infill         MH = Manufactured Housing         PD = Flexible diaphragm	Ves Final Level 2 Coore C	12				une s	uuciural s	system			de	etailed ev	aluation	is not ne	ecessary				
egend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry Infill MH = Manufactured Housing FD = Flexible diaphragm				IVI N	0							o, no nor	structura	al hazard	ts identifi	ed D	DNK		
egeno. Mint - Moment-ressung trame RC - Keningrou concrete UKM INK = Unreinforced masonry innii MH = Manulacured Housing FU = Hexible diaphragm BR = Braced frame SW = Shear wall TU = Tilt up LM = Light metal RD = Rigid diaphragm	Nonstructural hazards?	Yes		1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1													- 10 T 10 A 11		
	Nonstructural hazards?	Yes Prmation c		e verifie	d, scr					1990 - SPA 34	1. Sec. 13 8 384						83235 January		
	Nonstructural hazards?  Where info egend: MRF = 1	Yes Prmation c Moment-resis		e verifie e F	d, scr RC = R	einforced co			URMINE	= Unreinfo	1. Sec. 13 8 384		MH	= Manufa	ictured Ho	ousing Fl	D = Flexib	le diaphra diaphragn	gm 1
	Nonstructural hazards?  Where info egend: MRF = 1	Yes Prmation c Moment-resis		e verifie e F	d, scr RC = R	einforced co			URMINE	= Unreinfo	1. Sec. 13 8 384		MH	= Manufa	ictured Ho	ousing Fl	D = Flexib	le diaphra diaphragn	gm n
	Nonstructural hazards? X Where info egend: MRF = 1	Yes Prmation c Moment-resis		e verifie e F	d, scr RC = R	einforced co			URMINE	= Unreinfo	1. Sec. 13 8 384		MH	= Manufa	ictured Ho	ousing Fl	D = Flexib	le diaphra diaphragn	gm n

### Lathrop High School 1962 Addition

Level 1

#### Rapid Visual Screening of Buildings for Potential Seismic Hazards **HIGH Seismicity** FEMA P-154 Data Collection Form 901 Airport Way Address: Zip: 99701 Fairbanks, Alaska Other Identifiers Lathrop High School 1962 Addition **Building Name:** schoo Use: 64.8362 deg N 147.7328 deg W atitude: Longitude: 0.993 0.379 Ss: S1: Unit SMG February 201 Date/Time: Screener(s): Year Built: 1962 D EST No. Stories: Above Grade: Below Grade: C Code Year: 1958 Total Floor Area (sq. ft.): 000 Additions: None X Yes, Year(s) Built: 1957 1962, 1970 Historic Shelter Assembly Emer. Services Occupancy: Commercial From 1962 Industrial Office Government School Drawings Utility Warehouse Residential, # Units: KEY PLAN ПВ C DD DNK Soil Type: ΠE **□**F Soft If DNK, assume Type D. Hard Dense Poor Avg Rock Rock Soil Soil Soil Soil Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt.: Yes/No/DNK Pounding Falling Hazards from Taller Adjacent Building Adjacency: Vertical (type/severity) Irregularities: X Plan (type) Reentrant corner Unbraced Chimneys Heavy Cladding or Heavy Veneer Exterior Falling Hazards: Parapets Appendages Other: COMMENTS: SKETCH Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 S5 (URM INF) C3 (URM INF) FEMA BUILDING TYPE Do Not W1 W1A W2 S1 (MRF) S2 (BR) \$3 (LM) \$4 (RC C1 (MRF PC1 (TU) PC2 RM2 URM MH Know (FD) (RD) **Basic Score** 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vertical Irregularity, VL1 -1.2 -1.2 -1.2 -1.0 -1.0 -1.1 -1.0 -0.8 -0.9 -1.0 -0.7 -1.0 -0.9 -0.9 -0.9 -0.7 NA Moderate Vertical Irregularity, VL1 -0.7 -0.7 -0.7 -0.6 -0.7 -0.6 -0.5 -0.5 -0.6 -0.4 -0.5 -0.5 -0.4 NA -0.6 -0.6 -0.5 Plan Irregularity, PL1 -1.1 -1.0 -1.0 -0.8 -0.7 -0.9 -0.7 -0.6 -0.6 -0.8 -0.5 -0.7 -0.6 -0.7 -0.7 -0.4 NA Pre-Code -1.1 -1.0 -0.9 -0.6 -0.6 -0.8 -0.6 -0.2 -0.4 -0.7 -0.1 -0.5 -0.3 -0.5 -0.5 0.0 -0.1 Post-Benchmark 1.6 1.9 2.2 1.4 1.9 NA 1.9 2.1 NA 2.0 2.4 NA 1.2 1.4 1.1 2.1 2.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.5 0.3 0.3 Soil Type E (1-3 stories) 0.2 0.2 0.1 -0.2 -0.4 0.2 -0.1 -0.4 0.0 0.0 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2 -0.4 Soil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 -0.6 NA -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, SM 1.1 0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.3 0.2 0.2 0.3 0.3 0.2 1.0 1.2 1.0 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN ACTION REQUIRED EXTENT OF REVIEW **OTHER HAZARDS** Exterior: Partial All Sides 🔲 Aerial Are There Hazards That Trigger A **Detailed Structural Evaluation Required?** Х Yes, unknown FEMA building type or other building Yes, score less than cutoff Visible Entered Detailed Structural Evaluation? Interior: None Visi Yes No No geotech report Drawings Reviewed: 🔀 Pounding potential (unless S<sub>L2</sub> > Soil Type Source: cut-off, if known) Yes, other hazards present Geologic Hazards Source: No geotech report No No Falling hazards from taller adjacent Contact Person: building Detailed Nonstructural Evaluation Recommended? (check one) Geologic hazards or Soil Type F Yes, nonstructural hazards identified that should be evaluated LEVEL 2 SCREENING PERFORMED? Significant damage/deterioration to No, nonstructural hazards exist that may require mitigation, but a the structural system Yes, Final Level 2 Score, SL2 X No detailed evaluation is not necessary Nonstructural hazards? X Yes X No No. no nonstructural hazards identified X DNK Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know MRF = Moment-resisting frame BR = Braced frame MH = Manufactured LM = Light metal RC = Reinforced concret SW = Shear wall FD = Flexible diaphrag RD = Rigid diaphragm reinforced masonry infil Housing Legend TU = Tilt up Dennis L. Berry, PE Troy J. Feller, PE Colin Maynard, PE Scott M. Gruhn, PE **Greg Latreille, PE**

## Lathrop High School 1970 Addition

### **Rapid Visual Screening of Buildings for Potential Seismic Hazards** FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

Severe Vertical Irregularity, V1:       -1.2       -1.2       -1.2       -1.0       -1.0       -1.1       -1.0       -0.8       -0.9       -1.0       -0.7       -1.0       -0.7       -0.6       -0.6       -0.7       -0.6       -0.6       -0.7       -0.6       -0.6       -0.7       -0.6       -0.6       -0.7       -0.6       -0.6       -0.7       -0.6       -0.6       -0.7       -0.6       -0.6       -0.7       -0.6       -0.6       -0.6       -0.7       -0.6       -0.6       -0.6       -0.6       -0.6       -0.6       -0.7       -0.6       -0.7       -0.6       -0.7       -0.6       -0.7       -0.6       -0.7       -0.6       -0.7       -0.6       -0.7       -0.1       -0.7       -0.7       -0.6       -0.7       -0.6       -0.7       -0.7       -0.6       -0.7       -0.7       -0.6       -0.7       -0.7       -0.6       -0.7       -0.7<								Add	ress:			rport				0	0701				
Building Name:       Lattirtop Fight School 19/07 Addition         Description         Description <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>~</th> <th></th> <th>202.8</th> <th>airba</th> <th>TIKS, A</th> <th>Alask</th> <th>d</th> <th> Z</th> <th>Zip: 9</th> <th>9/01</th> <th></th> <th></th>								~		202.8	airba	TIKS, A	Alask	d	Z	Zip: 9	9/01				
Ust:											athro	p Hia	n Sc	hool 1	970	Addit	ion				
Lutiviz:       64.43822 deg N, unpublic:       1.7.7282 deg V, soggest sector of the sector o	Internet and the second	-	4		-	.1			•												
Screener(s):       Dust Time:       Extra Transmission         Screener(s):       Dust Time:       Extra Transmission       Extra Transmission         Screener(s):       Dust Time:       Transmission       Screener(s):       Dust Time:         Screener(s):       Dust Time:       Transmission       Screenerer       Screenerer       Dust Time:		mu			1	C Alexandra	-			6	4.836	2 deg	J N	Longitu	ide:			28 de	eg V		
No. Stories:       Above Grade:       Year Built:       Year Built: <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>10 A 10</td> <td></td> <td>-</td> <td></td> <td></td> <td>2</td> <td>S1:</td> <td>andeko - <del>20</del></td> <td>(in)</td> <td></td> <td></td> <td></td>		-						10 A 10		-			2	S1:	andeko - <del>20</del>	(in)					
Table Floor Area (p. ft):       ???       Cook Yes: 1967         Occupancy:       Assembly       Wes Naved by       Wes Naved by       Wes Naved by         Occupancy:       Assembly       Over Naved by       Bit Set Part Port Part Set Part Part Part Part Part Part Part Par						The		Scre	eener(s)	: <u>S</u>	MG		<i>w</i>	D	ate/Time	31 <del>.</del>					
Additions:       None       Yes, Yes(s) Built       192, 192, 192, 192, 192, 192, 192, 192,	and the second se					-							Belo	w Grade	e: 0				EST		
Occupancy:     Aseroby     Comments on separato page       Soil Type:													ear(s) l	Built:	1957.						
Induitie       One of the sector					-	-													ter		
Boil Type:       Image: Construction       Boil Type:       Image: Construction       Difference									0.0	Indu							Sovernmer	nt			
Hard       Avg       Develope       Set								0.1	-										-		
Adjacency:       Pendrage       Pendrage       Pendrage         Adjacency:       Pendrage       Pendrage       Pendrage         Adjacency:       Pendrage       Pendrage       Pendrage         Adjacency:       Pendrage       Pendrage       Pendrage         Pendrage       Pendrage       Pend					_			Soll	Type:									ите Туре	D.		
Adjacency:       Pounding       Faling Hazards from Taler Adjacent Building         Image: Second Seco						_												2.0	_		
Image: Second			_		-	_		_													
Image: Second		_	_	-		_		_			100 000 000 000 000 000 000 000 000 000	•			lazards fr	rom Talle	r Adjacen	t Building	3		
Line of the second s			_	-	-	-		irreg	gularitie	IS:					nt cor	rner					
Hazards:       Parapets       Parapets       Appendages         Other:       Other:       Other:       Other:         Dial       Other:       Other:       Other:         SECU       COMMENTS:       Drawings not available         Sector       Additional sketches or comments on separate page:         Exercise:       Comments:       Drawings not available         Sector       Additional sketches or comments on separate page:         Exercise:       Sector       Sector       Sector         Exercise:       Sector       Sector       Sector       Sector         Sector       Sector       Sector       Sector       Sector       Sector         Sector       Sector       Sector       Sector       Sector       Sector       Sector         Sector						_		Exte	erior Fal	lling							ding or H	eavy Ver	neer		
Comments:       Drawings not available         SETCH       Drawings not available         SETCH       Addoma sketches or comments on separate page.         Sector       Sector         Sector       Addoma sketches or comments on separate page.         Sector       Sector         Sector       Sector         Sector       Sector         Sector       Norm         <			_			_				ĩ	🗆 P	arapets									
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Additional sketches or comments on separate page         SKTM         Additional sketches or comments on separate page         SKTM         Chan Subches or comments on separate page         Stational sketches or comments of separate <td></td> <td></td> <td>_</td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td>not a</td> <td>vailat</td> <td>ole</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>			_			-					not a	vailat	ole								
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BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SLT           EMA BUILDING TYPE         Do Not Know         W1         W1 <th colspan="2" td="" w<=""><td></td><td></td><td></td><td></td><td>-</td><td>-</td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th>	<td></td> <td></td> <td></td> <td></td> <td>-</td> <td>-</td> <td></td> <td>-</td> <td></td>						-	-		-											
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Eth A BUILDING TYPE       Do Not       W1       W1       W2       S1       S2       S3       S4       S5       C1       C2       C3       PC1       PC2       RM1       RM2       URM       MM         Basic Score       3.6       3.2       2.9       2.1       2.0       2.6       2.0       1.7       1.5       2.0       1.2       1.6       1.4       1.7       1.7       1.0       0.9<		SKE	TCH						Additiona	al sketch	es or coi	mments o	n separ	rate page	1						
Know         (MRF)         (RR)         (MA)         (RC)         (MRF)         (MR				23 C C C C C C C C C C C C C C C C C C C																	
Bevere Vertical Irregularity, V1:       -12       -12       -12       -10       -10       -11       -10       -08       -09       -10       -07       -10       -09       -09       -09       -07       NA         Adderate Vertical Irregularity, V1:       -07       -07       -06       -05       -05       -05       -04       NA         Pain freqularity, P1:       -11       -10       -0.0       -0.7       -0.6       -0.5       -0.5       -0.5       -0.7       -0.6       -0.5       -0.7       -0.6       -0.5       -0.7       -0.6       -0.5       -0.7       -0.7       -0.4       NA         Yre-Code       -11       -10       -0.9       -0.6       -0.6       -0.6       -0.2       -0.4       -0.7       -0.1       -0.5       -0.3       -0.5	FEMA BUILDING TYPE		W1	W1A	W2				(RC	(URM			(URM		PC2			URM	мн		
Moderate Vertical Irregularity, Vr:       -0.7       -0.7       -0.6       -0.6       -0.5       -0.5       -0.4       -0.5       -0.5       -0.5       -0.5       -0.5       -0.5       -0.5       -0.5       -0.5       -0.5       -0.5       -0.5       -0.5       -0.7       -0.6       -0.7       -0.6	Basic Score		2.023	5.375	10000	-1225	0.505.5		62632	142322		And and a state of the local division of the local division of the local division of the local division of the	1000	1000	10000	the second se		1338			
Pre-Code       -1.1       -1.0       -0.9       -0.6       -0.8       -0.6       -0.2       -0.4       -0.7       -0.1       -0.5       -0.3       -0.5       0.0       0.1       1.2         Pre-Code       0.1       0.3       0.5       0.4       0.4       1.1       1.9       NA       1.9       2.1       NA       1.0       2.0       2.4       2.1       NA       1.0       2.0       2.4       2.1       NA       1.0       0.5       0.4       0.6       0.6       0.6       0.6       0.6       0.6       0.6       0.4       0.5       0.3       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.4       0.6       0.6       0.6       0.6       0.6       0.6       0.6       0.6       0.6       0.6       0.6       0.6       0.6       0.6       0	Moderate Vertical Irregularity, VL1		10000	0.0000			11.196.2		100.022	2022/04/04/04	12.12.2.2.2.2	2002		1836		1.	100.00		100000		
Prost-Benchmark       1.6       1.9       2.2       1.4       1.4       1.1       1.9       NA       1.9       2.1       NA       2.0       2.4       2.1       2.1       NA       1.2         Soli Type E (1-3 stories)       0.2       0.2       0.1       0.2       0.4       0.6       0.6       0.6       0.6 <td>Plan Irregularity, PL1</td> <td></td> <td>1053.57</td> <td>0.000</td> <td></td> <td>11 12 12 12 12 12 12</td> <td>2030320</td> <td></td> <td>100225</td> <td>102,822</td> <td>3320265</td> <td></td> <td>- CO 12</td> <td>- 1943 A.</td> <td>00000104</td> <td></td> <td>100000</td> <td>2022</td> <td>2014</td>	Plan Irregularity, PL1		1053.57	0.000		11 12 12 12 12 12 12	2030320		100225	102,822	3320265		- CO 12	- 1943 A.	00000104		100000	2022	2014		
Soil Type E (1-3 stories)       0.2       0.2       0.1       -0.2       -0.4       0.2       0.1       -0.4       0.0       0.0       -0.2       -0.3       -0.1       -0.1       -0.2       0.4         Soil Type E (1-3 stories)       -0.3       -0.6       -0.6       0.6       NA       -0.6       -0.4       -0.5       -0.7       -0.3       NA       -0.4       -0.5       -0.6       -0.6       -0.6       0.5	Pre-Code Post-Benchmark				10000	0.000	238232		10.000	88989 F	10202	10.03338			2122222	10.00000	22.24.22	19633	1000		
Soil Type E (> 3 stories)       -0.3       -0.6       -0.9       -0.6       0.6       NA       -0.5       -0.7       -0.3       NA       -0.4       -0.5       -0.7       -0.3       0.4       -0.5       -0.6       -0.2       NA         Minimum Score, Sumv       1.1       0.9       0.7       0.5       0.5       0.5       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.3       0.3       0.2       1.4         FINAL LEVEL 1 SCORE, SL12 SMW       1.1       0.9       0.7       0.5       0.5       0.6       0.5       0.5       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.2       0.3       0.3       0.	Soil Type A or B		0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3		
Minimum Score, Surv       1.1       0.9       0.7       0.5       0.5       0.5       0.5       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       0.2       0.3       0.3       0.2       1.0         EXTENT OF REVIEW         Exterior:       Partial       All Sides       Aerial       Entered       Detailed Structural Evaluation Required?       Partialed Structural Evaluation Required?       Partiales       Partiale Significant damage/deterioration to building       Partiales       Part	Soil Type E (1-3 stories) Soil Type E (> 3 stories)		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10.348	135522111		201203060		10000	2000	200000				000000	1.111224-031		C 2223	10.000		
ACTION REQUIRED         Exterior:       Partial       All Sides       Aerial         Interior:       None       Visible       Entered         Drawings Reviewed:       Yes       No         Soil Type Source:       No geotech report         Soil Type Source:       No geotech report         Geologic Hazards Source: No geotech report       Pounding potential (unless St2>         Contact Person:       Pologic hazards from taller adjacet         PK, Final Level 2 Score, St2       No         Yes, Final Level 2 Score, St2       No         Nonstructural hazards?       No         Were information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data <u>OF</u> DNK = Do Not Know         egend:       MF = Momentresisting frame       RC = Reinforced concrete       URM INF = Unreinforced masonry infill       MF = Manufactured Housing       PD = Rigid diaphragm         SW = Shear wall       TU = Tilt up       ME I Breved Housing       PD = Rigid diaphragm	Minimum Score, SMW									07.007		0.3		-			-				
Exterior:       Partial       All Sides       Aerial         Interior:       None       Visible       Entered         Drawings Reviewed:       Ves       No       Pounding potential (unless St2>         Soil Type Source:       No       geotech report       Pounding potential (unless St2>         Soil Type Source:       No       geotech report       Pounding potential (unless St2>         Soil Type Source:       No       geotech report       Pounding potential (unless St2>         Cut-off, if known)       Paling hazards from taller adjacent       No         Betailed Structural Evaluation Recommended?       (check one)         Petailed Structural bazards present       No         Betailed Structural bazards present       No         Contact Person:       Piss, final Level 2 Score, St2       No         Yes, Final Level 2 Score, St2       No       No         Wonstructural hazards?       Yes       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know         egend:       MRF = Moment-resisting frame       RC = Reinforced concrete       URM INF = Unrelinforced masonry infill       MH = Light metal       RD = Rigid diaphragm         BR = Braced frame       SW = Shear wail	FINAL LEVEL 1 SCORE, St	L1 ≥ Smin:										1.2				1.0					
Interior:       None       Visible       Entered         Drawings Reviewed:       Yes       No       Detailed Structural Evaluation?       Yes, unknown FEMA building type or other building         Soil Type Source:       No       Geotech report       Pounding potential (unless St.2 > cut-off, if known)       Yes, score less than cut-off         Soil Type Source:       No       Geotech report       Pounding potential (unless St.2 > cut-off, if known)       No         Contact Person:       Falling hazards form taller adjacent building       Geologic hazards or Soil Type F       No         LEVEL 2 SCREENING PERFORMED?       Xes, final Level 2 Score, St.2       Xes       No         Yes, Final Level 2 Score, St.2       Xo       No       Vestificant damage/deterioration to the structural system       No, nonstructural hazards identified that should be evaluated         Nonstructural hazards?       Yes       No       No       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know         egend:       MRF = Moment-resisting frame       RC = Reinforced concrete       URM INF = Unreinforced masonry infill       MH = Light metal       RD = Rigid diaphragm         BR = Braced frame       SW = Shear wail       TU = Tilt up       TU = Tilt up       RD = Rigid diaphragm	EXTENT OF REVIEW				Π	OTHE	RHAZ	ARDS			ACT	ION R	EQUI	RED							
Drawings Reviewed:       Yes       No         Soil Type Source:       No geotech report         Soil Type Source:       No geotech report         Scholl Type Source:       Pounding potential (unless Siz> cut-off, if known)         Contact Person:       Falling hazards from taller adjacent building         Geologic hazards or Soil Type F       Geologic hazards or Soil Type F         Level 2 SCREENING PERFORMED?       No         Yes, Final Level 2 Score, Siz       No         Nonstructural hazards?       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data OR DNK = Do Not Know         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data OR DNK = Do Not Know         BR = Braced frame       SW = Shear wall       TU = Tilt up										4	Detail	ed Struc	tural Ev	valuation	Require	ed?					
Soil Type Source:       No geotech report         Soil Type Source:       No geotech report         Seologic Hazards Source:       Cut-off, if known)         Soil Type Source:       Soil for source:         Soil for source:       Soil for source:         Soil for source:       Soil for source:         Soil for source:       No         Soil for source:       No         No       Soil for source:         Soil for source:       No         Soil for source:       No         Soil for source:       No         Source:       Soil for source:         Source	Interior: X Non Drawings Reviewed: Yes	e 🗌 V 🕅 N			ered						Y					or other b	uilding				
Geologic Hazards Source: No geotech report       Falling hazards from taller adjacent building       No         Contact Person:       Geologic hazards or Soil Type F       Ves, nonstructural hazards identified that should be evaluated the structural system       Ves, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary         Ves, Final Level 2 Score, Stage       No       No         Nonstructural hazards?       Yes       No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR       DNK = Do Not Know         egend:       MRF = Moment-resisting frame       RC = Reinforced concrete       URM INF = Unreinforced masonry infill       MH = Manufactured Housing       FD = Flexible diaphragm         BR = Braced frame       SW = Shear wall       TU = Tilt up       LM = Light metal       RD = Rigid diaphragm	Soil Type Source: No	o geote	ech re			cut-o	ff, if know	/n)			□ Y	es, other									
EVEL 2 SCREENING PERFORMED?       Geologic hazards or Soil Type F       Yes, nonstructural hazards identified that should be evaluated         Yes, Final Level 2 Score, Siz       No       Yes       No         Yonstructural hazards?       Yes       No       Yes         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR       DNK         Were information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR       DNK = Do Not Know         Were information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR       DNK = Do Not Know         Regend:       MR = Braced frame       RC = Reinforced concrete       URM INF = Unreinforced masonry infill       MH = Manufactured Housing       FD = Flexible diaphragm         BR = Braced frame       SW = Shear wall       TU = Tilt up       TU = Tilt up       EX = Light metal       RD = Rigid diaphragm		geote	ech re	eport		Fallir	ng hazard		aller adja	icent											
Yes, Final Level 2 Score, S <sub>L2</sub> No         Yes, Final Level 2 Score, S <sub>L2</sub> No         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR       DNK         Where information cannot be verified, screener shall note the following:       EST = Estimated or unreliable data       OR       DNK         Regend:       MRF = Moment-resisting frame       RC = Reinforced concrete       URM INF = Unreinforced masonry infill       MH = Manufactured Housing       FD = Flexible diaphragm         SW = Shear wall       TU = Tilt up       TU = Tilt up       RD = Rigid diaphragm	1949-000 (1949-000) (1949-000) (1949-000) (1949-000) (1949-000) (1949-000) (1949-000) (1949-000) (1949-000) (19				=	Geol	ogic haza				1.12.23.23.2										
If es, Final Level 2 scole, 32       Image: Scole, 32<		11112000000	ORME						terioratio	on to	N	o, nonstr	uctural h	nazards e	exist that						
Where information cannot be verified, screener shall note the following:         EST = Estimated or unreliable data         OR         DNK = Do Not Know           Legend:         MRF = Moment-resisting frame BR = Braced frame         RC = Reinforced concrete SW = Shear wall         URM INF = Unreinforced masonry infill TU = Tilt up         MH = Manufactured Housing LM = Light metal         PD = Flexible diaphragm RD = Rigid diaphragm		1000				100	. actor of a									ied f					
egend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm BR = Braced frame SW = Shear wall TU = Tilt up LM = Light metal RD = Rigid diaphragm		192720	annot h	1.1		eener sha	ll note th	e follow	ina: FS	ST = Esti	-	- 1. J 1 1 1 1 1 1				100 <b>-</b>					
BR = Braced frame SW = Shear wall TU = Tilt up LM = Light metal RD = Rigid diaphragm	Legend: MRF = M			ie I	RC = Re	einforced co		1	URM INF :	= Unreinfo			MH	I = Manufa	actured Ho	ousing F	D = Flexib	le diaphra	igm		
nnie I. Permy DE – Troy I. Faller, DE – Colin Maymend, DE – Coatt M. Crutha, DE – Craad atmille, D					0111 01	lane an anall		131	THE - THE	10			1 M	= 1 ight m	etal		D - Diald	dianhraan	n		
nnia   Parmy DE - Tray   Fallar DE - Calin Maymerry DE - Saatt M. Crytha DE - Cryst I straille D	BK = BU			1	SW = SI	riear waii			ro = nicu	ik.			LIN	Lightin	U.C.	6	KD = Rigia	ulaphilagh			
nnia   Parry DE Tray   Fallar DE Calin Maymerd DE Saatt M. Crythin DE Const Attaille D	BK = Br				SW = SI	near wali			10 - 111 u	μ			Lin	Light in			KD = Kigia	uapinagn			
	BK = Br			i	5W = 5I	near wan			10 - 1110	Ψ			Lin	Light in			KD – Kigia	uapiragn			

### North Pole Elementary School 1967 Original Construction

#### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

250 Snowman Lane Address: North Pole, Alaska 99705 Zip: Other Identifiers: North Pole Elementary School 1967 Original **Building Name:** schoo Use: 64.7521 deg N 147.3494 deg W \_atitude: Longitude: 0.983 0.378 Ss: S1: SMG February 2017 Date/Time: Screener(s): Year Built: 1967 D EST No. Stories: Above Grade: Below Grade: 0 43 .000 Code Year: 1964 Total Floor Area (sq. ft.): Additions: X None Yes, Year(s) Built: Assembly Commercial Emer. Services Historic Shelter Occupancy: Industrial Office School Government Utility Warehouse Residential, # Units: ПВ ПC DD □F DNK Soil Type: ΠE Soft If DNK, assume Type D. Hard Avg Dense Poor Rock Rock Soil Soil Soil Soil Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt.: Yes/No/DNK Pounding Falling Hazards from Taller Adjacent Building Adjacency: Vertical (type/severity) rregularities: X Plan (type) Reentrant corner Unbraced Chimneys Heavy Cladding or Heavy Veneer Exterior Falling Hazards: Parapets Appendages Other: COMMENTS: Contains both wood stud shear walls and CMU shear walls SKETCH Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 S5 (URM INF) C3 (URM INF) FEMA BUILDING TYPE Do Not W1 W1A S1 (MRF) S2 (BR) \$3 (LM) S C1 (MRF C2 PC1 (TU) PC2 RM1 (FD) RM2 URM MH (RC Know (SW) (RD) **Basic Score** 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vertical Irregularity, VL1 -1.2 -1.2 -1.2 -1.0 -1.0 -1.1 -1.0 -0.8 -0.9 -1.0 -0.7 -1.0 -0.9 -0.9 -0.9 -0.7 NA Moderate Vertical Irregularity, VL1 -0.7 -0.7 -0.7 -0.6 -0.7 -0.6 -0.5 -0.5 -0.6 -0.4 -0.5 -0.5 -0.4 NA -0.6 -0.6 -0.5 Plan Irregularity, PL1 -1.1 -1.0 -1.0 -0.8 -0.7 -0.9 -0.7 -0.6 -0.6 -0.8 -0.5 -0.7 -0.6 -0.7 -0.7 -0.4 NA Pre-Code -1.1 -1.0 -0.9 -0.6 -0.6 -0.8 -0.6 -0.2 -0.4 -0.7 -0.1 -0.5 -0.3 -0.5 -0.5 0.0 -0.1 2.1 Post-Benchmark 1.6 1.9 2.2 1.4 1.9 NA 1.9 NA 2.0 2.4 2.1 NA 1.2 1.4 1.1 2.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.5 0.3 0.3 Soil Type E (1-3 stories) 0.2 0.2 0.1 -0.2 -0.4 0.2 -0.1 -0.4 0.0 0.0 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2 -0.4 Soil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 -0.6 NA -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, SM 1.1 0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.3 0.2 0.2 0.3 0.3 0.2 1.0 1.9 1.0 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: ACTION REQUIRED EXTENT OF REVIEW OTHER HAZARDS Exterior: Partial 🔀 All Sides 🗌 Aerial Are There Hazards That Trigger A **Detailed Structural Evaluation Required?** Yes, unknown FEMA building type or other building Yes, score less than cut-off Visi Visible D Entered Detailed Structural Evaluation? Interior: None Interior: Drawings Reviewed: X Yes No Self Type Source: No geotech report Pounding potential (unless S<sub>12</sub> > cut-off, if known) Yes, other hazards present Geologic Hazards Source: No geotech report Falling hazards from taller adjacent No No Contact Person: building Detailed Nonstructural Evaluation Recommended? (check one) Geologic hazards or Soil Type F Yes, nonstructural hazards identified that should be evaluated LEVEL 2 SCREENING PERFORMED? Significant damage/deterioration to No, nonstructural hazards exist that may require mitigation, but a the structural system Yes, Final Level 2 Score, SL2 X No detailed evaluation is not necessary Nonstructural hazards? X No X Yes No. no nonstructural hazards identified X DNK Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know FD = Flexible diaphrag RD = Rigid diaphragm MRF = Moment-resisting frame BR = Braced frame MH = Manufactured Housing LM = Light metal RC = Reinforced concrete SW = Shear wall URM INF = Unreinforced masonry infill Legend TU = Tilt up Dennis L. Berry, PE Troy J. Feller, PE Colin Maynard, PE Scott M. Gruhn, PE **Greg Latreille, PE** 

## North Pole Middle School 1975 Original Construction

### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

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FEMA BUILDING TYPE Do No Knov	1	W1A	W2	<b>S1</b> (MRF)	<b>S2</b> (BR)	\$3 (LM)	<b>\$4</b> (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	мн
Basic Score Severe Vertical Irregularity, VL1	3.6 -1.2	3.2 -1.2	2.9 -1.2	2.1 -1.0	2.0 -1.0	<b>2.6</b> -1.1	<b>2.0</b> -1.0	1.7 -0.8	1.5 -0.9	2.0 -1.0	1.2 -0.7	1.6 -1.0	1.4 -0.9	1.7 -0.9	<b>1.7</b> -0.9	1.0 -0.7	1.5 NA
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	-0.6	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.7	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0	-0.8	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Pre-Code Post-Benchmark	-1.1 1.6	-1.0 1.9	-0.9 2.2	-0.6 1.4	-0.6 1.4	-0.8 1.1	-0.6 1.9	-0.2 NA	-0.4 1.9	-0.7 2.1	-0.1 NA	-0.5 2.0	-0.3 2.4	-0.5 2.1	-0.5 2.1	0.0 NA	-0.1 1.2
Soil Type A or B	0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories)	0.2	0.2	0.1 -0.9	-0.2	-0.4 -0.6	0.2 NA	-0.1 -0.6	-0.4 -0.4	0.0 -0.5	0.0 -0.7	-0.2 -0.3	-0.3 NA	-0.1 -0.4	-0.1 -0.5	-0.1 -0.6	-0.2 -0.2	-0.4 NA
Soil Type E (> 3 stories) Minimum Score, Smw	-0.3	-0.6	-0.9	-0.6	-0.6	0.6	-0.6	-0.4	-0.5	-0.7	-0.3	0.2	-0.4	-0.5	-0.6	-0.2	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MI}$	v:	3					9.1							1.0	1.0		
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nterior: 🛛 None	Visible			Detailed				5		es, unkno					uildina		
Drawings Reviewed: 🗌 Yes 🛛 🗙 Soil Type Source: No geo	No tech r	eport		Pour			nless SL2	>	🗙 Ye	es, score	less than	n cut-off					
Geologic Hazards Source: No geo					ff, if knov ig hazard		aller adia	icent		es, other l o	nazards	present					
Contact Person:		1		build	ing					ed Nonst	ructural	Evalua	tion Rec	ommen	ded? (ch	eck one)	
LEVEL 2 SCREENING PERI	ORME	D?			ogic haza ficant dai				□ Y	es, nonstr	uctural h	azards i	dentified	that sho	ould be ev	valuated	
Yes, Final Level 2 Score, St2		X N	0		tructural		038036585	C. 1997 (C.		o, nonstru etailed eva				may req	uire mitig	ation, bu	la
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	n cannot k	1.000	d, scre	eener shal	I note th	e follow	ring: ES	ST = Esti	imated o	or unrelia	ble data	OR	DNK = D	o Not K	now		
Nonstructural hazards? Xes Where information Legend: MRF = Moment-r	esisting fran	be verifie	RC = Re	einforced co		1	URM INF	= Unreinfo			MH	= Manufa	ctured Ho	using F	D = Flexib	le diaphra	gm
Nonstructural hazards? Xes Where information	esisting fran	be verifie	RC = Re			1		= Unreinfo			MH		ctured Ho	using F		le diaphra diaphragn	gm n
Nonstructural hazards? Xes Where information Legend: MRF = Moment-r	esisting fran	be verifie	RC = Re	einforced co		1	URM INF	= Unreinfo			MH	= Manufa	ctured Ho	using F	D = Flexib	le diaphra diaphragn	gm n
Nonstructural hazards? Xes Where information Legend: MRF = Moment-r	esisting fran	be verifie	RC = Re	einforced co		1	URM INF	= Unreinfo			MH	= Manufa	ctured Ho	using F	D = Flexib	le diaphra diaphragn	gm n
Nonstructural hazards? X Yes Where information Legend: MRF = Moment BR = Braced fram	esisting fran	be verifie	RC = Re SW = St	einforced co near wall	ncrete		URM INF	= Unreinfo p	vrced mas		MH : LM =	= Manufa = Light me	ctured Ho etal	using F F	D = Flexib	diaphragn	n

## Tanana Middle School 1974 Original Construction

### Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

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FEMA BUILDING TYPE	Do Not	W1	W1A	W2	S1	S2	S3	\$4	S5	C1	C2	C3	PC1	PC2	RM1	RM2	URM	МН
	Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)		(FD)	(RD)		
Basic Score		3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1		-1.2	-1.2	-1.2	10.000	-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1		-0.7 -1.1	-0.7 -1.0	-0.7 -1.0	2012/02	-0.6 -0.7	-0.7 -0.9	-0.6 -0.7	-0.5 -0.6	-0.5	-0.6 -0.8	-0.4 -0.5	-0.6 -0.7	-0.5 -0.6	-0.5	-0.5 -0.7	-0.4 -0.4	NA NA
Pre-Code		-1.1	-1.0	-0.9	10.1	-0.6	-0.9	-0.6	-0.0	-0.6	-0.0	-0.5	-0.7	-0.0	-0.5	-0.5	0.0	-0.1
Post-Benchmark		1.6	1.9	2.2		1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type A or B		0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories)		0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Soil Type E (> 3 stories) Minimum Score, Skow		-0.3	-0.6 0.9	-0.9	-0.6	-0.6	NA 0.6	-0.6 0.5	-0.4 0.5	-0.5	-0.7 0.3	-0.3 0.3	NA 0.2	-0.4 0.2	-0.5 0.3	-0.6 0.3	-0.2	NA 1.0
Constant and the second second second		5.1	0.9	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0	0.2	0.2	1.0	0.0	0.2	1.0
FINAL LEVEL 1 SCORE, SL	1 2 3MIN.														1.0			
EXTENT OF REVIEW					OTHE	R HAZ	ARDS	;		ACT	ION R	EQUI	RED					
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Drawings Reviewed: X Yes Soil Type Source: NO	geote		eport			nding pot		nless SL2	>		es, score					100		
Geologic Hazards Source: No	<u>×</u>	_	_			off, if kno ng hazar		aller adia	cent		es, other	nazards	present					
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LEVEL 2 SCREENING		JRME				ificant da structural		eterioratio	on to		lo, nonstr							ta
Yes, Final Level 2 Score, Sta	1997 - Contra 19		X N		ule s	Auctural	system				etailed ev							
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## West Valley High School 1976 Original Construction

Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

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South Wing	10	1 1	10.1				No.	Stories:	Abov	e Grade	2	Belov	w Grade	: 0	Year	Built:	976	EST
South wing	140	20		TTF	1111		Tota	I Floor	Area (so	. ft.):	114	,000			Code	Year:	1973	
Center Print	· 120	<b>\$</b> \$\$	1	十字	Same 1		Add	itions:	X N	one 🗌	] Yes, '	Year(s) B	uilt:		32		A DESCRIPTION OF THE REAL PROPERTY OF THE REAL PROP	
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FEMA BUILDING TYPE	Do Not	W1	W1A	W2	RE, MO	S2	S3	S4	<b>S</b> 5	C1	C2	C3	PC1	PC2	RM1	RM2	URM	мн
	Know			65226	(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)		(FD)	(RD)		CONS.
Basic Score		3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
		-1.2 -0.7	-1.2 -0.7	-1.2 -0.7	-1.0 -0.6	-1.0 -0.6	-1.1 -0.7	-1.0 -0.6	-0.8 -0.5	-0.9 -0.5	-1.0 -0.6	-0.7 -0.4	-1.0 -0.6	-0.9 -0.5	-0.9 -0.5	-0.9 -0.5	-0.7 -0.4	
		-0.1	10.000	-0.7	-0.8	-0.6		0.0		-0.0	-0.0	10.4	-0.6	10.000		0.0	0.4	10000
Inderate Vertical Irregularity, VL1		-1.1	-1.0				-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.1	-0.6	-0.7	-0.7	-0.4	NA
Noderate Vertical Irregularity, VL1 Nan Irregularity, PL1		-1.1 -1.1	-1.0	-0.9	-0.6	-0.6	-0.9 -0.8	-0.7 -0.6		-0.6 -0.4	-0.8 -0.7	-0.5 -0.1	-0.7	-0.6 -0.3		-0.7 -0.5	-0.4 0.0	NA NA NA -0.1
loderate Vertical Irregularity, VL; lan Irregularity, PL; re-Code ost-Benchmark		-1.1 1.6	-1.0 1.9	-0.9 2.2	-0.6 1.4	1.4	-0.8 1.1	-0.6 1.9	-0.6 -0.2 NA	-0.4 1.9	-0.7 2.1	-0.1 NA	-0.5 2.0	-0.3 2.4	-0.7 -0.5 2.1	-0.5 2.1	0.0 NA	NA NA -0.1 1.2
toderate Vertical Irregularity, V <sub>L1</sub> Ian Irregularity, P <sub>L1</sub> re-Code rost-Benchmark ioil Type A or B		-1.1 1.6 0.1	-1.0 1.9 0.3	-0.9 2.2 0.5	-0.6 1.4 0.4	1.4 0.6	-0.8 1.1 0.1	-0.6 1.9 0.6	-0.6 -0.2 NA 0.5	-0.4 1.9 0.4	-0.7 2.1 0.5	-0.1 NA 0.3	-0.5 2.0 0.6	-0.3 2.4 0.4	-0.7 -0.5 2.1 0.5	-0.5 2.1 0.5	0.0 NA 0.3	NA NA -0.1 1.2 0.3
loderate Vertical Irregularity, V <sub>L1</sub> lan Irregularity, P <sub>L1</sub> re-Code ost-Benchmark oil Type A or B oil Type E (1-3 stories)		-1.1 1.6 0.1 0.2	-1.0 1.9 0.3 0.2	-0.9 2.2 0.5 0.1	-0.6 1.4 0.4 -0.2	1.4 0.6 -0.4	-0.8 1.1 0.1 0.2	-0.6 1.9 0.6 -0.1	-0.6 -0.2 NA 0.5 -0.4	-0.4 1.9 0.4 0.0	-0.7 2.1 0.5 0.0	-0.1 NA 0.3 -0.2	-0.5 2.0 0.6 -0.3	-0.3 2.4 0.4 -0.1	-0.7 -0.5 2.1 0.5 -0.1	-0.5 2.1 0.5 -0.1	0.0 NA 0.3 -0.2	NA -0.1 1.2 0.3 -0.4
Ioderate Vertical Irregularity, $V_{Lf}$ lan Irregularity, $P_{Lf}$ re-Code ost-Benchmark oil Type A or B oil Type E (1-3 stories) oil Type E (> 3 stories)		-1.1 1.6 0.1	-1.0 1.9 0.3	-0.9 2.2 0.5	-0.6 1.4 0.4 -0.2 -0.6	1.4 0.6 -0.4 -0.6	-0.8 1.1 0.1 0.2 NA	-0.6 1.9 0.6 -0.1 -0.6	-0.6 -0.2 NA 0.5	-0.4 1.9 0.4 0.0 -0.5	-0.7 2.1 0.5 0.0 -0.7	-0.1 NA 0.3 -0.2 -0.3	-0.5 2.0 0.6 -0.3 NA	-0.3 2.4 0.4 -0.1 -0.4	-0.7 -0.5 2.1 0.5 -0.1 -0.5	-0.5 2.1 0.5 -0.1 -0.6	0.0 NA 0.3	NA -0.1 1.2 0.3 -0.4 NA
Ioderate Vertical Irregularity, VL1 Ian Irregularity, PL1 re-Code ost-Benchmark oil Type A or B oil Type E (1-3 stories) oil Type E (2-3 stories) ilinimum Score, SMN	.1 ≥ Smin:	-1.1 1.6 0.1 0.2 -0.3	-1.0 1.9 0.3 0.2 -0.6	-0.9 2.2 0.5 0.1 -0.9	-0.6 1.4 0.4 -0.2	1.4 0.6 -0.4	-0.8 1.1 0.1 0.2	-0.6 1.9 0.6 -0.1	-0.6 -0.2 NA 0.5 -0.4 -0.4	-0.4 1.9 0.4 0.0	-0.7 2.1 0.5 0.0	-0.1 NA 0.3 -0.2	-0.5 2.0 0.6 -0.3	-0.3 2.4 0.4 -0.1	-0.7 -0.5 2.1 0.5 -0.1	-0.5 2.1 0.5 -0.1	0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Adderate Vertical Irregularity, $V_{L1}$ Irregularity, $P_{L1}$ irre-Code Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Inimium Score, Sway FINAL LEVEL 1 SCORE, $S_{L1}$	.1 ≥ Smin:	-1.1 1.6 0.1 0.2 -0.3	-1.0 1.9 0.3 0.2 -0.6	-0.9 2.2 0.5 0.1 -0.9	-0.6 1.4 0.4 -0.2 -0.6	1.4 0.6 -0.4 -0.6 0.5 <b>1.3</b>	-0.8 1.1 0.1 0.2 NA 0.6	-0.6 1.9 0.6 -0.1 -0.6 0.5	-0.6 -0.2 NA 0.5 -0.4 -0.4	-0.4 1.9 0.4 0.0 -0.5 0.3	-0.7 2.1 0.5 0.0 -0.7 0.3	-0.1 NA 0.3 -0.2 -0.3	-0.5 2.0 0.6 -0.3 NA 0.2 0.9	-0.3 2.4 0.4 -0.1 -0.4	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	-0.5 2.1 0.5 -0.1 -0.6	0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Moderate Vertical Irregularity, V⊥1           Plan Irregularity, P⊥1           Pre-Code           Post-Benchmark           Soil Type A or B           Soil Type E (1-3 stories)           Soil Type E (2-3 stories)           Winimum Score, SMW           FINAL LEVEL 1 SCORE, SL:           EXTENT OF REVIEW           Exterior:         □ Partia	ial 🔀 A	-1.1 1.6 0.1 0.2 -0.3 1.1	-1.0 1.9 0.3 0.2 -0.6 0.9	-0.9 2.2 0.5 0.1 -0.9 0.7	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHER Are There	1.4 0.6 -0.4 -0.6 0.5 1.3 HAZ	-0.8 1.1 0.1 0.2 NA 0.6	-0.6 1.9 0.6 -0.1 -0.6 0.5	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.4 1.9 0.4 0.0 -0.5 0.3	-0.7 2.1 0.5 0.0 -0.7 0.3	-0.1 NA 0.3 -0.2 -0.3 0.3	-0.5 2.0 0.6 -0.3 NA 0.2 0.9	-0.3 2.4 0.4 -0.1 -0.4 0.2	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 <b>1.0</b>	-0.5 2.1 0.5 -0.1 -0.6	0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Partia Mone	ial 🔀 A e 🗌 V	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides /isible	-1.0 1.9 0.3 0.2 -0.6 0.9	-0.9 2.2 0.5 0.1 -0.9 0.7	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHER Are There Detailed S	1.4 0.6 -0.4 -0.6 0.5 1.3 HAZZA	-0.8 1.1 0.1 0.2 NA 0.6 ARDS s That T al Evalu	-0.6 1.9 0.6 -0.1 -0.6 0.5	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.4 1.9 0.4 0.0 -0.5 0.3	-0.7 2.1 0.5 0.0 -0.7 0.3	-0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation	-0.3 2.4 0.4 -0.1 -0.4 0.2	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 <b>1.0</b>	-0.5 2.1 0.5 -0.1 -0.6 0.3	0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Moderate Vertical Irregularity, VL) Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SL; EXTENT OF REVIEW Exterior: Partice Interior: None Drawings Reviewed: X Yes	ial 🗙 A e 🗌 V	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides /isible	-1.0 1.9 0.3 0.2 -0.6 0.9 Aeria	-0.9 2.2 0.5 0.1 -0.9 0.7	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHEF Are There Detailed S Pound	1.4 0.6 -0.4 -0.6 0.5 1.3 HAZZ	-0.8 1.1 0.1 0.2 NA 0.6 ARDS s That T al Evalu ntial (un	-0.6 1.9 0.6 -0.1 -0.6 0.5	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.4 1.9 0.4 0.0 -0.5 0.3 <b>ACT</b> Detaile	-0.7 2.1 0.5 0.0 -0.7 0.3	-0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF etural Ev own FEN	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation IA buildir n cut-off	-0.3 2.4 0.4 -0.1 -0.4 0.2	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 <b>1.0</b>	-0.5 2.1 0.5 -0.1 -0.6 0.3	0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Interior: X None Drawings Reviewed: X Yes Soil Type Source: NO	ial X A e U V D geote	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides /isible No ech re	-1.0 1.9 0.3 0.2 -0.6 0.9 Aeria Enter eport	-0.9 2.2 0.5 0.1 -0.9 0.7	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHEF Are There Detailed S Pounc cut-of	1.4 0.6 -0.4 -0.6 0.5 1.3 Hazard Structura ding pote f, if know	-0.8 1.1 0.2 NA 0.6 ARDS s That 1 al Evalu ntial (un m)	-0.6 1.9 0.6 -0.1 -0.6 0.5	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.4 1.9 0.4 0.0 -0.5 0.3 ACT Detaile Ye X Ye Y Ye	-0.7 2.1 0.5 0.0 -0.7 0.3	-0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation IA buildir n cut-off	-0.3 2.4 0.4 -0.1 -0.4 0.2	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 <b>1.0</b>	-0.5 2.1 0.5 -0.1 -0.6 0.3	0.0 NA 0.3 -0.2 -0.2	NA -0.1 1.2 0.3 -0.4 NA
Moderate Vertical Irregularity, V⊥ Plan Irregularity, P⊥ Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, Swaw FINAL LEVEL 1 SCORE, SL EXTENT OF REVIEW Exterior: □ Partite Interior: ☑ None Drawings Reviewed: ☑ Yes	ial X A e U V D geote	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides /isible No ech re	-1.0 1.9 0.3 0.2 -0.6 0.9 Aeria Enter eport	-0.9 2.2 0.5 0.1 -0.9 0.7	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHEF Are There Detailed S Pound	1.4 0.6 -0.4 -0.6 0.5 1.3 HAZ/ Hazards Structura ding pote f, if know g hazards	-0.8 1.1 0.2 NA 0.6 ARDS s That 1 al Evalu ntial (un m)	-0.6 1.9 0.6 -0.1 -0.6 0.5	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.4 1.9 0.4 0.0 -0.5 0.3 <b>ACT</b> Detaile Detaile Ye Ye No	-0.7 2.1 0.5 0.0 -0.7 0.3 ION R ed Structes, unknies, score es, other	-0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF etural Ev bown FEM less tha hazards	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation NA buildir n cut-off present	-0.3 2.4 0.4 -0.1 -0.4 0.2 Require	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 1.0	-0.5 2.1 0.5 -0.1 -0.6 0.3	0.0 NA 0.3 -0.2 -0.2 0.2	NA -0.1 1.2 0.3 -0.4 1.0
Moderate Vertical Irregularity, VL) Plan Irregularity, PL) Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SL) EXTENT OF REVIEW EXTERTOF REVIEW Exterior: Partice Interior: Partice Soil Type Source: No Geologic Hazards Source: No	ial X A e V <u>o geote</u> o geote	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides Visible No Poch re	-1.0 1.9 0.3 0.2 -0.6 0.9 Aeria Enter eport	-0.9 2.2 0.5 0.1 -0.9 0.7	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHEF Are There Detailed S Pound cut-of Fallin buildit Geold	1.4 0.6 -0.4 -0.6 0.5 1.3 Hazard Structura ding pote f, if know g hazard 19 gic haza	-0.8 1.1 0.1 0.2 NA 0.6 ARDS s That T al Evalu ntial (un m) s from ta rds or S	-0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A ation? allers S <sub>L2</sub> aller adja coil Type	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 0.5	-0.4 1.9 0.4 0.0 -0.5 0.3 <b>ACT</b> Detaile Ye Ye No Detaile	-0.7 2.1 0.5 0.0 -0.7 0.3	-0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev bwn FEM less tha hazards	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation IA buildir n cut-off present	-0.3 2.4 0.4 -0.1 -0.4 0.2 Require	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 1.0 r other bu	-0.5 2.1 0.5 -0.1 -0.6 0.3	0.0 NA 0.3 -0.2 -0.2 0.2	NA -0.1 1.2 0.3 -0.4 NA 1.0
Moderate Vertical Irregularity, VL) Pare-Tregularity, PL) Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, Sum FINAL LEVEL 1 SCORE, SL) EXTENT OF REVIEW Exterior: Partice Interior: Partice Soil Type Source: No Geologic Hazards Source: No Contact Person: LEVEL 2 SCREENING	ial X A e V geote geote	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides Visible No Poch re	-1.0 1.9 0.3 0.2 -0.6 0.9 Aeria Enter eport eport D?	-0.9 2.2 0.5 0.1 -0.9 0.7 al red	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHEF Are There Detailed S Pounc cut-of Fallin buildi Geolo Signif	1.4 0.6 -0.4 -0.6 0.5 1.3 Hazard: Structura ding pote f, if know g hazard: ng gic haza icant dan	-0.8 1.1 0.1 0.2 NA 0.6 ARDS s That T al Evalu ntial (un m) s from ta rds or S nage/de	-0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A ation? allers S <sub>L2</sub>	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 0.5	-0.4 1.9 0.4 0.0 -0.5 0.3 ACT Detaile Ye No Detaile Detaile Ye	-0.7 2.1 0.5 0.0 -0.7 0.3 ION R ed Struct es, unknown es, score s, other o ed Nons es, nonst	-0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev bwn FEM less tha hazards tructural	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation IA buildir n cut-off present I Evalua	-0.3 2.4 0.4 -0.1 -0.4 0.2 Require og type o	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 1.0	-0.5 2.1 0.5 -0.1 -0.6 0.3	0.0 NA 0.3 -0.2 -0.2 0.2	NA NA -0.1 1.2 0.3 -0.4 NA 1.0
Moderate Vertical Irregularity, VL; I'an Irregularity, PL; Pre-Code Post-Benchmark Soil Type A or B Soil Type E (-3 stories) Soil Type E (-3 stories) Soil Type E (-3 stories) FINAL LEVEL 1 SCORE, SL; EXTENT OF REVIEW Exterior: □ Partia Therior: ○ None Soil Type Source: ○ None Soil Type Sou	ial X A e V D geote D geote PERFC	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides Visible No Poch re	-1.0 1.9 0.3 0.2 -0.6 0.9 Aeria Enter eport eport D? No	-0.9 2.2 0.5 0.1 -0.9 0.7 al red	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHEF Are There Detailed S Pounc cut-of Fallin buildi Geolo Signif	1.4 0.6 -0.4 -0.6 0.5 1.3 Hazard Structura ding pote f, if know g hazard 19 gic haza	-0.8 1.1 0.1 0.2 NA 0.6 ARDS s That T al Evalu ntial (un m) s from ta rds or S nage/de	-0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A ation? allers S <sub>L2</sub> aller adja coil Type	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 0.5	-0.4 1.9 0.4 0.0 -0.5 0.3 ACT Detaile Ye Ye Ve Detaile Detaile No Detaile Deta	-0.7 2.1 0.5 0.0 -0.7 0.3 ION R ed Struct es, unknuss, score es, unknuss, score es, other o d Nons es, nonstl o, nonstl	-0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev bown FEN less tha hazards tructural luctural luctural hazards	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation IA buildir n cut-off present I Evalua hazards e is not ne	-0.3 2.4 0.4 -0.1 -0.4 0.2 Require g type o tion Rec dentified xist that cessary	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 1.0 r other bu	-0.5 2.1 0.5 -0.1 -0.6 0.3 iilding iilding	0.0 NA 0.3 -0.2 -0.2 0.2	NA NA -0.1 1.2 0.3 -0.4 NA 1.0
Adderate Vertical Irregularity, VL1 Pre-Code	ial X A e V geote geote PERFC	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides Visible No ech re ech re	-1.0 1.9 0.3 0.2 -0.6 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	-0.9 2.2 0.5 0.1 -0.9 0.7	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHER Are There Detailed 3 Pount cut-of Fallin buildi Geold Signif the st	1.4 0.6 -0.4 -0.6 0.5 1.3 HAZ/ HAZ/ HAZ/ HAZ/ Hazard Structura ding pote f, if know g hazard ng gic haza icant dan ructural s	-0.8 1.1 0.2 NA 0.6 ARDS s That 1 al Evalu ntial (un n) s from ta rds or S nage/de system	-0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A ation? nless S <sub>L2</sub> aller adja soil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	-0.4 1.9 0.4 0.0 -0.5 0.3 ACT Detaile Yee Not Detaile Yee Not Detaile Not Detaile	-0.7 2.1 0.5 0.0 -0.7 0.3 <b>ION R</b> ed Struct es, unknies, score es, store es, store ses, other of ad Nons ses, nonstr tailed ew o, no nor	-0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev own FEN less tha hazards tructural l uctural h valuation nstructura	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation IA buildir n cut-off present I Evalua hazards e is not ne al hazard	-0.3 2.4 0.4 -0.1 -0.4 0.2 Require ag type o tion Rec identified xist that cessary s identified	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 1.0 ad? r other bu	-0.5 2.1 0.5 -0.1 -0.6 0.3 iilding iilding	0.0 NA 0.3 -0.2 -0.2 0.2	NA NA -0.1 1.2 0.3 -0.4 NA 1.0
Moderate Vertical Irregularity, V⊥ Pare-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (2 3 stories) Minimum Score, Skew FINAL LEVEL 1 SCORE, SL: EXTENT OF REVIEW Exterior: □ Partice Soil Type Source: □ Partice Soil Type Source: ○ None Geologic Hazards Source: No Contact Person: LEVEL 2 SCREENING □ Yes, Final Level 2 Score, SL: Nonstructural hazards? ∑	ial X A e V D geote D	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides Visible No ech re ech re cannot b	-1.0 1.9 0.3 0.2 -0.6 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	-0.9 2.2 0.5 0.1 -0.9 0.7	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHER Are There Detailed 3 Poun cut-of Fallin buildi Geolo Signif the st	1.4 0.6 -0.4 -0.6 0.5 1.3 HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/	-0.8 1.1 0.1 0.2 NA 0.6 ARDS s That T s	-0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A ation? aller adja oil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 0.5	-0.4 1.9 0.4 0.0 -0.5 0.3 ACT Details Yee No Details Mo Details No Details Details No Details	-0.7 2.1 0.5 0.0 -0.7 0.3 <b>CON R</b> <b>CON R</b> <b>CON</b>	-0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF tural Ev bwn FEM less tha hazards tructural uctural hazards tructural uctural dual tructural uctural dual tructural uctural uctural tructural	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation IA buildir n cut-off present I Evalua hazards azards e is not ne al hazard	-0.3 2.4 0.4 -0.1 -0.4 0.2 Require ag type of tion Rec dentified xist that cessary s identifi DNK = D	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 1.0 ad? r other bu commence it that sho may required by Not Krin	-0.5 2.1 0.5 -0.1 -0.6 0.3 iilding iilding iilding iild be ev ire mitig: DNK	0.0 NA 0.3 -0.2 -0.2 0.2	NA NA -0.1 1.2 0.3 -0.4 1.0 1.0
Adderate Vertical Irregularity, VL1 Pre-Code Pre-Code Pre-Code Soil Type A or B Soil Type E (1-3 stories) Soil Type E (2-3 stories) Alinimum Score, Skew FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Partia Therior: None Drawings Reviewed: Yes Soil Type Source: No Seologic Hazards Sourc	ial X A e V D geote D geote PERFC	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides Visible No ech re ech re cannot b	-1.0 1.9 0.3 0.2 -0.6 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	-0.9 2.2 0.5 0.1 -0.9 0.7 al red 	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHER Are There Detailed S Pound cut-of Fallin buildit Geolo Signif the st	1.4 0.6 -0.4 -0.6 0.5 1.3 HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/	-0.8 1.1 0.1 0.2 NA 0.6 ARDS s That 1 al Evalu ntial (un n) s from ta rds or S nage/de system e follow	-0.6 1.9 0.6 -0.1 -0.6 0.5 <b>Trigger A</b> <b>ation?</b> nless S <sub>L2</sub> aller adja ioil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7	-0.4 1.9 0.4 0.0 -0.5 0.3 ACT Details Yee No Details Mo Details No Details Details No Details	-0.7 2.1 0.5 0.0 -0.7 0.3 <b>CON R</b> <b>CON R</b> <b>CON</b>	-0.1 NA 0.3 -0.2 -0.3 EQUIF trural Ev own FEM less tha hazards tructural l uctural h valuation structural maturation	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation IA buildir n cut-off present I Evalua hazards e is not ne al hazards al hazards	-0.3 2.4 0.4 -0.1 -0.4 0.2 Require gr type o tion Rec dentified xist that cessary s identifi DNK = D	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 1.0 ad? r other but ad? r other but ad? r other but ad? r other but adv adv adv adv adv adv adv adv adv adv	-0.5 2.1 0.5 -0.1 -0.6 0.3 iilding iilding ire mitig: DNK tow = Flexib	0.0 NA 0.3 -0.2 -0.2 0.2 valuated ation, but	NA NA -0.1 1.2 0.3 -0.4 NA 1.0
foderate Vertical Irregularity, PL1         Irregularity, PL1         Irre-Code         ost-Benchmark         Soil Type A or B         Soil Type E (1-3 stories)         Soil Type E (2-3 stories)         Itinimum Score, Skow         FINAL LEVEL 1 SCORE, SL1         EXTENT OF REVIEW         Exterior:       Partia         Drawings Reviewed:       Yes         Scologic Hazards Source:       None         Scologic Hazards Source:       None         Scologic Hazards Source:       None         Scologic Hazards Source:       None         Where infor       Where infor	ial X A e V D geote D	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides Visible No ech re ech re cannot b	-1.0 1.9 0.3 0.2 -0.6 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	-0.9 2.2 0.5 0.1 -0.9 0.7 al red 	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHER Are There Detailed 3 Poun cut-of Fallin buildi Geold Signif the st	1.4 0.6 -0.4 -0.6 0.5 1.3 HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/	-0.8 1.1 0.1 0.2 NA 0.6 ARDS s That 1 al Evalu ntial (un n) s from ta rds or S nage/de system e follow	-0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger A ation? aller adja oil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7	-0.4 1.9 0.4 0.0 -0.5 0.3 ACT Details Yee No Details Mo Details No Details Details No Details	-0.7 2.1 0.5 0.0 -0.7 0.3 <b>CON R</b> <b>CON R</b> <b>CON</b>	-0.1 NA 0.3 -0.2 -0.3 EQUIF trural Ev own FEM less tha hazards tructural l uctural h valuation structural maturation	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation IA buildir n cut-off present I Evalua hazards azards e is not ne al hazard	-0.3 2.4 0.4 -0.1 -0.4 0.2 Require gr type o tion Rec dentified xist that cessary s identifi DNK = D	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 1.0 ad? r other but ad? r other but ad? r other but ad? r other but adv adv adv adv adv adv adv adv adv adv	-0.5 2.1 0.5 -0.1 -0.6 0.3 iilding iilding ire mitig: DNK tow = Flexib	0.0 NA 0.3 -0.2 -0.2 0.2	NA NA -0.1 1.2 0.3 -0.4 NA 1.0
foderate Vertical Irregularity, PL1         Irregularity, PL1         Irre-Code         ost-Benchmark         Soil Type A or B         Soil Type E (1-3 stories)         Soil Type E (2-3 stories)         Itinimum Score, Skow         FINAL LEVEL 1 SCORE, SL1         EXTENT OF REVIEW         Exterior:       Partia         Drawings Reviewed:       Yes         Scologic Hazards Source:       None         Scologic Hazards Source:       None         Scologic Hazards Source:       None         Scologic Hazards Source:       None         Where infor       Where infor	ial X A e V D geote D geote PERFC	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides Visible No ech re ech re cannot b	-1.0 1.9 0.3 0.2 -0.6 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	-0.9 2.2 0.5 0.1 -0.9 0.7 al red 	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHER Are There Detailed S Pound cut-of Fallin buildit Geolo Signif the st	1.4 0.6 -0.4 -0.6 0.5 1.3 HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/	-0.8 1.1 0.1 0.2 NA 0.6 ARDS s That 1 al Evalu ntial (un n) s from ta rds or S nage/de system e follow	-0.6 1.9 0.6 -0.1 -0.6 0.5 <b>Trigger A</b> <b>ation?</b> nless S <sub>L2</sub> aller adja ioil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7	-0.4 1.9 0.4 0.0 -0.5 0.3 ACT Details Yee No Details Mo Details No Details Details No Details	-0.7 2.1 0.5 0.0 -0.7 0.3 <b>CON R</b> <b>CON R</b> <b>CON</b>	-0.1 NA 0.3 -0.2 -0.3 EQUIF trural Ev own FEM less tha hazards tructural l uctural h valuation structural maturation	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation IA buildir n cut-off present I Evalua hazards e is not ne al hazards al hazards	-0.3 2.4 0.4 -0.1 -0.4 0.2 Require gr type o tion Rec dentified xist that cessary s identifi DNK = D	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 1.0 ad? r other but ad? r other but ad? r other but ad? r other but adv adv adv adv adv adv adv adv adv adv	-0.5 2.1 0.5 -0.1 -0.6 0.3 iilding iilding ire mitig: DNK tow = Flexib	0.0 NA 0.3 -0.2 -0.2 0.2 valuated ation, but	NA NA -0.1 1.2 0.3 -0.4 NA 1.0 t a
Adderate Vertical Irregularity, VL1 Pre-Code Pre-Code Pre-Code Soil Type A or B Soil Type E (1-3 stories) Soil Type E (2-3 stories) Alinimum Score, Skew FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Partia Therior: None Drawings Reviewed: Yes Soil Type Source: No Seologic Hazards Sourc	ial X A e V D geote D geote PERFC	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides Visible No ech re ech re cannot b	-1.0 1.9 0.3 0.2 -0.6 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	-0.9 2.2 0.5 0.1 -0.9 0.7 al red 	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHER Are There Detailed S Pound cut-of Fallin buildit Geolo Signif the st	1.4 0.6 -0.4 -0.6 0.5 1.3 HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/ HAZ/	-0.8 1.1 0.1 0.2 NA 0.6 ARDS s That 1 al Evalu ntial (un n) s from ta rds or S nage/de system e follow	-0.6 1.9 0.6 -0.1 -0.6 0.5 <b>Trigger A</b> <b>ation?</b> nless S <sub>L2</sub> aller adja ioil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.4 -0.5 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7	-0.4 1.9 0.4 0.0 -0.5 0.3 ACT Details Yee No Details Mo Details No Details Details No Details	-0.7 2.1 0.5 0.0 -0.7 0.3 <b>CON R</b> <b>CON R</b> <b>CON</b>	-0.1 NA 0.3 -0.2 -0.3 EQUIF trural Ev own FEM less tha hazards tructural l uctural h valuation structural maturation	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation IA buildir n cut-off present I Evalua hazards e is not ne al hazards al hazards	-0.3 2.4 0.4 -0.1 -0.4 0.2 Require gr type o tion Rec dentified xist that cessary s identifi DNK = D	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 1.0 ad? r other but ad? r other but ad? r other but ad? r other but adv adv adv adv adv adv adv adv adv adv	-0.5 2.1 0.5 -0.1 -0.6 0.3 iilding iilding ire mitig: DNK tow = Flexib	0.0 NA 0.3 -0.2 -0.2 0.2 valuated ation, but	NA NA -0.1 1.2 0.3 -0.4 NA 1.0
Moderate Vertical Irregularity, V <sub>2</sub> ; Plan Irregularity, P <sub>2</sub> ; Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (2 3 stories) Minimum Score, S <sub>460</sub> <b>FINAL LEVEL 1 SCORE, S<sub>2</sub>;</b> <b>EXTENT OF REVIEW</b> Exterior: Partia Interior: None Drawings Reviewed: Yes Soil Type Source: No Geologic Hazards Source: O Contact Person: LEVEL 2 SCREENING Yes, Final Level 2 Score, S <sub>2</sub> ; Nonstructural hazards? None Where infor egend: MRF = M	ial A A e V geote geote geote geote performation c Moment-resis aced frame	-1.1 1.6 0.1 0.2 -0.3 1.1 All Sides Visible No each ree each ree cannot b cannot b	-1.0 1.9 0.3 0.2 -0.6 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	-0.9 2.2 0.5 0.1 -0.9 0.7 al red 1, scree C = Re W = Sh	-0.6 1.4 0.4 -0.2 -0.6 0.5 OTHER Are There Detailed S Pound cut-of Falling building Geolog Signif the st Pound Cut-of Signif the st	1.4 0.6 -0.4 -0.6 0.5 1.3 <b>R HAZ</b> /d Hazard ding pote f, if know g hazard gigc haza ccant dan g gigc haza ccant dan to to to to to to to to to to to to to	-0.8 1.1 0.1 0.2 NA 0.6 ARDS s That 1 exactly a second se	-0.6 1.9 0.6 -0.1 -0.6 0.5 <b>Trigger A</b> <b>ation?</b> nless S <sub>L2</sub> aller adja ioil Type terioratio	-0.6 -0.2 NA 0.5 -0.4 -0.4 0.5 	-0.4 1.9 0.4 1.9 0.0 -0.5 0.3 Detaile Y Ye Not Detaile Y Ye Not Detaile Y Ye Not Commated o Not	-0.7 2.1 0.5 0.0 0.7 0.3 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-0.1 NA 0.3 -0.2 -0.3 EQUIF trural Ev own FEM less tha hazards tructural l uctural h valuation structural maturation	-0.5 2.0 0.6 -0.3 NA 0.2 0.9 RED aluation A buildir n cut-off present I Evalua azards is azards e is not ne al hazard	-0.3 2.4 0.4 -0.1 -0.4 0.2 Require gg type o tion Rec dentified xist that cessary s identified xist that DCLURE HO	-0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 1.0 ad? r other but ad? r other but ad? r other but ad? r other but ad?	-0.5 2.1 0.5 -0.1 -0.6 0.3 -0.6 0.3 -0.6 0.3 -0.6 0.3 -0.6 0.3 -0.6 0.3 -0.6 0.3 -0.6 0.3 -0.6 0.3 -0.6 0.3 -0.6 0.3 -0.6 0.3 -0.6 0.5 -0.1 -0.6 0.5 -0.1 -0.6 0.5 -0.1 -0.6 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5	0.0 NA 0.3 -0.2 -0.2 0.2 valuated ation, but	NA NA -0.1 1.2 0.3 -0.4 NA 1.0 1.0

#### Woodriver Elementary School 1976 Original Construction

Rapid Visual Screening of Buildings for Potential Seismic Hazards FEMA P-154 Data Collection Form

### Level 1 HIGH Seismicity

5000 Palo Verde Avenue Address: Fairbanks, Alaska 99709 Zip: PLAN ADDITIVE NORTH Other Identifiers BLOCK B Woodriver Elementary School 1976 Original **Building Name:** schoo Use: 64.8394 deg N 147.8706 deg W Latitude: Longitude: 0.998 0.381 Ss: S1: ATCH SMG February 201 Date/Time: Screener(s): No. Stories: Above Grade: Below Grade: 0 Year Built: 1976 C EST BLOCK Code Year: 1973 Total Floor Area (sq. ft.): 000 Additions: X None Yes, Year(s) Built: Assembly Commercial Emer. Services Historic Shelter Occupancy: Industrial Office School Government KEY PLAN Utility Warehouse Residential, # Units ПВ C DNK Soil Type: ΠE **□**F Avg If DNK, assume Type D. Hard Dense Soft Poor Rock Rock Soil Soil Soil Soil Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt.: Yes/No/DNK Pounding Falling Hazards from Taller Adjacent Building Adjacency: 8 Vertical (type/severity) Irregularities: X Plan (type) Reentrant corner Unbraced Chimneys Heavy Cladding or Heavy Veneer Exterior Falling 1 EL 401.17 Hazards: Parapets Appendages / TL 460 25 Other: COMMENTS: Steel x-bracing at penthouse. Precast concrete parapets sit atop CMU walls to resist lateral loads from roof above, but 0 3 this may create Stratys. LG-34-A COV Mar Shear 2.14 a hinge between -HE MC ON THE the top of CMU BAL WESS P and bottom of PRECAST PARAPET & GYMNASIUM (1) precast. SECTION (12) (15) AL CONST (14) Additional sketches or cor SECTION BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 S5 (URM INF) C3 (URM INF) FEMA BUILDING TYPE Do Not W1 W1A W2 S1 (MRF) \$3 (LM) S C1 (MRF C2 (SW) PC2 RM1 (FD) RM2 (RD) URM MH PC1 (TU) (RC Know (BR) Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vertical Irregularity, VL1 -1.2 -1.2 -1.2 -1.0 -1.0 -1.1 -1.0 -0.8 -0.9 -1.0 -0.7 -1.0 -0.9 -0.9 -0.9 -0.7 NA Moderate Vertical Irregularity, VL1 -0.7 -0.7 -0.7 -0.6 -0.7 -0.6 -0.5 -0.5 -0.6 -0.4 -0.5 -0.5 -0.4 NA -0.6 -0.6 -0.5 Plan Irregularity, PL1 -1.1 -1.0 -1.0 -0.8 -0.7 -0.9 -0.7 -0.6 -0.6 -0.8 -0.5 -0.7 -0.6 -0.7 -0.7 -0.4 NA Pre-Code -1.1 -1.0 -0.9 -0.6 -0.6 -0.8 -0.6 -0.2 -0.4 -0.7 -0.1 -0.5 -0.3 -0.5 -0.5 0.0 -0.1 2.1 Post-Benchmark 1.6 1.9 2.2 1.4 1.9 NA 1.9 NA 2.0 NA 1.2 1.4 1.1 2.4 2.1 2.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.5 0.3 0.3 Soil Type E (1-3 stories) 0.2 0.2 0.1 -0.2 -0.4 0.2 -0.1 -0.4 0.0 0.0 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2 -0.4 Soil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 -0.6 NA -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, SM 1.1 0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.3 0.2 0.2 0.3 0.3 0.2 1.0 2.0 0.9 1.0 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN ACTION REQUIRED EXTENT OF REVIEW OTHER HAZARDS Exterior: Partial All Sides 🗌 Aerial Are There Hazards That Trigger A **Detailed Structural Evaluation Required?** Yes, unknown FEMA building type or other building Yes, score less than cut-off Visible Entered Detailed Structural Evaluation? Interior: None Visi Yes No No geotech report Drawings Reviewed: 🔀 Pounding potential (unless SL2 > Soil Type Source: cut-off, if known) Yes, other hazards present Geologic Hazards Source: No geotech report Falling hazards from taller adjacent No No Contact Person: building Detailed Nonstructural Evaluation Recommended? (check one) Geologic hazards or Soil Type F Yes, nonstructural hazards identified that should be evaluated LEVEL 2 SCREENING PERFORMED?  $\overline{\Box}$ Significant damage/deterioration to No, nonstructural hazards exist that may require mitigation, but a the structural system Yes, Final Level 2 Score, SL2 X No detailed evaluation is not necessary Nonstructural hazards? X No X Yes No. no nonstructural hazards identified X DNK Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know MRF = Moment-resisting frame BR = Braced frame MH = Manufactured Housing LM = Light metal RC = Reinforced concre SW = Shear wall FD = Flexible diaphrag RD = Rigid diaphragm nforced masonry infil Legend TU = Tilt up Dennis L. Berry, PE Troy J. Feller, PE Colin Maynard, PE Scott M. Gruhn, PE **Greg Latreille, PE**